

C3. Air Quality Report



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Dixie Road Widening (Queen Street to 2 KM North of Mayfield Road) – Region of Peel Brampton, Ontario

Final Report

Air Quality Assessment

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EXECUTIVE SUMMARY

The **Region of Peel (the Region)** is undertaking the planning and preliminary design for the widening of Dixie Road from the Queen Street to 2 km north of Mayfield Road in the Region of Peel,

RWDI AIR Inc. (RWDI) was retained by AECOM to conduct an air quality assessment of the proposed improvements. The objective of the assessment was to quantify air contaminant emissions from vehicular traffic along, entering, exiting, and crossing Dixie Road and to determine how these emissions will affect air quality in the vicinity of the proposed upgrades. The detailed scope of this study is listed below:

- Identify the contaminants of interest;
- Use representative historical monitoring data to establish background concentrations for each contaminant, i.e., concentrations that are due to other emission sources in the area besides those associated with the project;
- Use vehicle emissions modelling techniques to predict tailpipe and road dust emissions associated with the project-related traffic, for the future build scenario (2031).
- Use a computer simulation of atmospheric dispersion to predict maximum contaminant concentrations at representative sensitive receptors due to emissions from project-related traffic, for the future build scenario.
- Combine the maximum predicted incremental concentrations attributable to the roadway with reasonable maximum background concentrations and assess the results relative to applicable ambient air quality guidelines.

As a screening-level approach, the study examined four main contaminants of concern for motor vehicles, specifically: carbon monoxide (CO), oxides of nitrogen (NO_x) including nitrogen dioxide (NO₂), inhalable (coarse) particulate matter (PM₁₀), and respirable (fine) particulate matter (PM_{2.5}).

The air quality assessment used maximum emission rates (winter condition), worst-case meteorological conditions based on a 1-hour simulation period, and reasonable worst-case background concentrations (90th percentile). The conclusions of the assessment can be summarized as follows:

- Incremental pollutant concentrations attributable to the roadway are much lower than background pollutant concentrations, and, when combined with representative high background concentrations (90th percentile level), are below the applicable thresholds.
- PM₁₀ was the contaminant with the highest percentage of its respective standard.
- The collective results indicate that overall, air quality is acceptable and the potential for unacceptable health impacts due to the project is low.



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1. INTRODUCTION

The **Region of Peel (the Region)** is undertaking the planning and preliminary design for the widening of Dixie Road from the Queen Street to 2 km north of Mayfield Road in the Region of Peel,

RWDI AIR Inc. (RWDI) was retained by AECOM to conduct an air quality assessment of the proposed improvements. The objective of the assessment was to quantify air contaminant emissions from vehicular traffic along, entering, exiting, and crossing Dixie Road and to determine how these emissions will affect air quality in the vicinity of the proposed upgrades. The detailed scope of this study is listed below:

- Identify the contaminants of interest;
- Use representative historical monitoring data to establish background concentrations for each contaminant, i.e., concentrations that are due to other emission sources in the area besides those associated with the project;
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- Use a computer simulation of atmospheric dispersion to predict maximum contaminant concentrations at representative sensitive receptors due to emissions from project-related traffic, for the future build scenario.
- Combine maximum predicted incremental concentrations attributable to the roadway with reasonable worst-case background concentrations and assess the results relative to applicable ambient air quality guidelines.

2. STUDY AREA

This study area consists of a mixture of residential and commercial areas at the south end of the study area, primarily residential areas through the centre of the study area, and a mixture of residential and open land at the north end of the study area. As can be seen from Figures 1 to 3, the residential areas are found on both the east and west sides of Dixie Road. Air quality impacts were assessed at 26 sensitive locations (known as sensitive receptors). These receptors were selected to represent worst-case impacts at sensitive locations surrounding the project area. A sensitive receptor was defined as a residence, church, school, hospital, daycare, or senior housing facility. The receptor locations are labelled R1 through R26 on Figures 1 to 3.

3. PROJECT DESCRIPTION

The purpose of the project is to address existing operational concerns and future transportation needs by considering a widening of existing Dixie Road beginning from the intersection of Queen Street to 2 km north of Mayfield Road in the City of Brampton. Detailed design changes and proposed improvements include:

1. Widening of the existing Dixie Road (3 lanes) beginning at the intersection of the Queen Street to the intersection of Country Side Drive
2. Widening of the existing Dixie Road (2 lanes) beginning at the intersection of the Country Side Drive to 2 km north of Mayfield Road
3. New exiting and entering turning lanes for many of the side roads which intersect Dixie Road.

Table 3.1 shows the traffic volumes, percentage of Heavy Duty Vehicles (HDV) and posted speeds at different intersections of the proposed study area. The posted speed limit along the Dixie Road varies from 60 km/h to 80 km/hr. The new widening will bring the road closer to the main residential developments, as they exist on both sides of the road.



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Table 3.1: Traffic Volumes and Posted Speeds for the Proposed Study Area for the Year 2031

| Name | Northbound Traffic | | Southbound Traffic | | Posted Speed (km/hr) |
|--|--------------------|-------|--------------------|-------|----------------------|
| | Volumes (AADT) | % HDV | Volumes (AADT) | % HDV | |
| Dixie Road South of Queen Street | 28540 | 8% | 17660 | 1% | 60 |
| Dixie Road South of Hillside Drive | 26200 | 7% | 12780 | 1% | 60 |
| Dixie Road South of Hazelwood Drive | 25550 | 3% | 12470 | 1% | 60 |
| Dixie Road South of Howden Blvd | 25340 | 3% | 12410 | 2% | 60 |
| Dixie Road South of Lascelles Blvd | 23520 | 3% | 11280 | 2% | 60 |
| Dixie Road South of Williams Pkwy | 22230 | 4% | 11240 | 1% | 60 |
| Dixie Road South of Northampton Street | 21630 | 2% | 10250 | 1% | 60 |
| Dixie Road South of North Park Drive | 19610 | 1% | 10130 | 1% | 60 |
| Dixie Road South of Northcliff Street-Moregate | 18260 | 3% | 10440 | 1% | 60 |
| Dixie Road South of Bovaird Drive | 17670 | 2% | 9870 | 3% | 60 |
| Dixie Road South of Peter Robertson Blvd | 24430 | 5% | 10330 | 1% | 60 |
| Dixie Road South of Springtown Trail | 21700 | 4% | 8100 | 2% | 60 |
| Dixie Road South of Sandalwood Pkwy | 20760 | 3% | 8420 | 3% | 60 |
| Dixie Road South of Octillo Blvd | 16990 | 3% | 10530 | 6% | 60 |
| Dixie Road South of Father Tobin Rd | 16230 | 12% | 9500 | 2% | 60 |
| Dixie Road South of Countryside Drive | 17050 | 3% | 8540 | 3% | 60 |
| Dixie Road South of Mayfield Road | 17020 | 7% | 11350 | 2% | 80 |
| Dixie Road North of Mayfield Road | 15180 | 2% | 14740 | 2% | 80 |

Notes:

% HDV – The percentage of Heavy Duty Vehicles (based on actual count data)

Traffic volumes shown are for major roads and highways only

Please see Figures 1 to 3 for Traffic details

4. CONTAMINANTS OF INTEREST

Vehicular traffic produces a variety of air contaminants as a result of combustion of fuel inside the engine, evaporation of fuel from the tank, brake and tire wear, and re-suspension (also known as re-entrainment) of material on the road surface (silt) as the vehicle travels over the road surface. The selected contaminants represent those that are typically of the greatest concern to Provincial and Federal regulatory authorities and are those typically associated with local human health or regional smog. Table 4.1 outlines the Chemical Compounds of Concern (CoCs).



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Table 4.1: Chemical Compounds of Concern

| Contaminant | Symbol or Chemical Formula |
|-------------------------------|---------------------------------|
| Carbon Monoxide | CO |
| Nitrogen Dioxide | NO ₂ |
| Respirable Particulate Matter | PM _{2.5} |
| Inhalable Particulate Matter | PM ₁₀ |
| Benzene | C ₆ H ₆ |
| 1-3 Butadiene | C ₄ H ₆ |
| Formaldehyde | CH ₂ O |
| Acetaldehyde | CH ₃ CHO |
| Acrolein | C ₃ H ₄ O |

5. RELEVANT GUIDELINES

The Ontario Ministry of the Environment (MOE) has developed Ambient Air Quality Criteria (AAQCs) for numerous pollutants, including those that are typically emitted from vehicular traffic and are known to have the potential to cause human health or environmental impacts [1]. Environment Canada (EC) has established National Ambient Air Quality Objectives (NAAQOs) for some of the same pollutants [2]. In general, these objectives represent desirable or acceptable ambient pollutant levels. Finally, the Canadian Council of Ministers of the Environment (CCME) developed a Canada Wide Standard (CWS) for PM_{2.5} [3]. The CWS for PM_{2.5} was established for the year 2010 and is based on the 98th percentile ambient measurement (24-hour) annually averaged over three consecutive years.

These aforementioned air quality criteria, objectives and standards are collectively referred to as air quality thresholds in this report. The thresholds used to assess potential impacts from transportation projects are summarized in Table 5.1. It should be noted that these values represent the concentrations in ambient air that are considered acceptable and protective of human health. They are not specifically enforceable for motor vehicle emissions within any of the jurisdictions.

Table 5.1: Summary of Relevant Air Quality Thresholds (µg/m³)

| Pollutant | Criterion (µg/m ³) | Averaging Period | Source | Reference |
|-------------------|--------------------------------|------------------|-----------------|-----------|
| PM _{2.5} | 30 | 24-hour | CWS | [3] |
| | 30 | 24-hour | AAQC | [1] |
| PM ₁₀ | 50 | 24-hour | AAQC | [1] |
| CO | 36,200 | 1-hour | AAQC | [1] |
| | 15,700 | 8-hour | AAQC | [1] |
| NO ₂ | 400 | 1-hour | AAQC | [1] |
| | 200 | 24-hour | AAQC | [1] |
| Benzene | 2.3 | 24-hour | AAQC (proposed) | [4] |
| | 0.45 | Annual | AAQC (proposed) | [4] |
| 1,3-Butadiene | 10 | 24-hour | AAQC (proposed) | [5] |
| | 2 | Annual | AAQC (proposed) | [5] |
| Acrolein | 4.5 | 1-hour | AAQC | [6] |
| | 0.4 | 24-hour | AAQC | [6] |



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| Pollutant | Criterion ($\mu\text{g}/\text{m}^3$) | Averaging Period | Source | Reference |
|--------------|--|------------------|--------|-----------|
| Acetaldehyde | 500 | 30-minute | AAQC | [1] |
| | 500 | 24-hour | AAQC | [1] |
| Formaldehyde | 65 | 24-hour | AAQC | [1] |

Prior to the dispersion modelling, the CoCs shown in Table 5.1 were screened to identify a short list of CoC for further analysis. The CoCs of greatest concern are those that have a combination of relatively low health-based threshold and relatively high emission rates from motor vehicles. Table 5.2 compares typical future motor vehicle emission rates to health-based AAQCs applicable to a 24-hour averaging period. The ranking shows that those having the highest emission rates relative to the criterion are benzene, NO_x , particulate matter (PM_{10} and $\text{PM}_{2.5}$), CO and 1,3-butadiene. In the case of benzene and 1,3-butadiene, however, the AAQC is a proposed threshold that has not yet been formally adopted.

Table 5.2: Ranking of CoCs

| Pollutant | Criterion ($\mu\text{g}/\text{m}^3$) | Average Vehicle Emission Rate in 2021 (g/km) [1] | Rank |
|-------------------|--|--|------|
| $\text{PM}_{2.5}$ | 30 | 0.03 | 4 |
| PM_{10} | 50 | 0.1 | 2 |
| CO | 15,700 | 3.7 | 6 |
| NO_x | 200 | 0.3 | 3 |
| Benzene | 2.3 | 0.006 | 1 |
| 1,3-Butadiene | 10 | 0.0006 | 5 |
| Acrolein | 4.5 | 0.0001 | 7 |
| Acetaldehyde | 500 | 0.0007 | 8 |
| Formaldehyde | 65 | 0.002 | 9 |

Notes:

[1] Emission rates based on 60 km/h, 6% heavy duty vehicles and winter conditions.

For the detailed assessment, NO_2 , particulate matter ($\text{PM}_{2.5}$ and PM_{10}) and CO were carried forward to represent all CoC's for the dispersion modelling.

6. BACKGROUND AIR QUALITY CONDITIONS

Background air pollutant levels, due to emissions from other sources besides the project-related sources in the Dixie Road study area can be generally characterized with air quality monitoring data from Ontario Ministry of Environment (MOE) [8]. There is one air quality monitoring station in proximity to the study area, located in Brampton, Ontario (MOE Station No. 46089) at 525 Main Street North/Peel Manor. This station is located in an urban setting, and is near the study area (approximately 4km from the study area), as such, the station should provide reasonably representative levels for estimating background concentrations. However, data for CO was not available for certain years from this site. In those cases, data were taken from the nearest monitoring site with data available (Toronto West – MOE Station No. 35125).

Table 6.1 provides a description of the stations used for the contaminants referenced in Section 4 and Table 6.2 provides a summary of the data. The mean values are representative of typical conditions, 90th percentile values (exceeded only 10% of the time) are representative of credible worst-case conditions, and maximum values are representative of rare peak events.



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Typical measured values reported in Table 6.2 result from a combination of local, regional and transboundary sources. In the case of PM_{2.5}, most elevated levels are associated with regional smog events involving complex photochemical processes. According to the MOE's "Air Quality in Ontario – 2005 Report" and "Transboundary Air Quality in Ontario – 2005 Report", transboundary air pollution (mainly from the United States) is one of the largest contributors to Ontario's smog events in the summer.

Table 6.1: Ambient Station Information

| Contaminant | Station ID | City | Location | Year |
|-----------------------|------------|--------------|------------------------------|-----------|
| CO | MOE #46089 | Brampton | Main Street North/Peel Manor | 2003-2004 |
| | MOE #35125 | Toronto West | Resources Road | 2005-2007 |
| NO ₂ | MOE #46089 | Brampton | Main Street North/Peel Manor | 2003-2007 |
| PM _{2.5} [1] | MOE #46089 | Brampton | Main Street North/Peel Manor | 2003-2007 |
| PM ₁₀ [2] | N/A | N/A | N/A | N/A |

Table 6.2: Summary of Ambient Air Measurements (µg/m³)

| Pollutant | Statistic | 2003 | 2004 | 2005 | 2006 | 2007 | Average |
|--|----------------------------|------|------|------|------|------|---------|
| CO (µg/m ³) | 1-hr Max | 6230 | 4134 | 3194 | 3591 | 1711 | 3772 |
| | 8-hr Max | 2808 | 2567 | 2000 | 2989 | 1061 | 2285 |
| | Annual Mean | 819 | 615 | 458 | 422 | 313 | 525 |
| | 1hr-90th Percentile | 1133 | 1097 | 759 | 663 | 530 | 836 |
| | Times > 1-hr AAQC (36,200) | 0 | 0 | 0 | 0 | 0 | 0 |
| | Times > 8-hr AAQC (15,700) | 0 | 0 | 0 | 0 | 0 | 0 |
| NO ₂ (µg/m ³) | 1-hr Max | 162 | 172 | 176 | 148 | 123 | 156 |
| | 24-hr Max | 115 | 105 | 107 | 83.2 | 75.2 | 97 |
| | Annual Mean | 34.8 | 32.1 | 33.5 | 29.9 | 27.5 | 32 |
| | 1hr-90th Percentile | 73.3 | 67.3 | 71.3 | 65.3 | 59.4 | 67 |
| | Times > 1-hr AAQC (200) | 0 | 0 | 0 | 0 | 0 | 0 |
| | Times > 24-hr AAQC (100) | 0 | 0 | 0 | 0 | 0 | 0 |
| PM _{2.5} (µg/m ³) | 1-hr Max | 64.0 | 65.0 | 59.0 | 51.0 | 65.0 | 61 |
| | 24-hr Max | 42.0 | 39.0 | 48.0 | 33.0 | 39.0 | 40 |
| | Annual Mean | 8.2 | 7.7 | 8.8 | 7.2 | 7.4 | 8 |
| | 24hr-90th Percentile | 18.0 | 18.0 | 22.0 | 16.0 | 17.0 | 18 |
| | Times > CWS (30) | 7 | 10 | 12 | 2 | 5 | 7 |



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| Pollutant | Statistic | 2003 | 2004 | 2005 | 2006 | 2007 | Average |
|--|----------------------------|-------|-------|-------|------|-------|---------|
| PM ₁₀ (µg/m ³) [1] | 1-hr Max | 118.5 | 120.4 | 109.3 | 94.4 | 120.4 | 113 |
| | 24-hr Max | 77.8 | 72.2 | 88.9 | 61.1 | 72.2 | 74 |
| | Annual Mean | 15.2 | 14.3 | 16.3 | 13.3 | 13.7 | 15 |
| | 24hr-90th Percentile | 33.3 | 33.3 | 40.7 | 29.6 | 31.5 | 34 |
| | Times > 24-hr AAQC (50) | n/a | n/a | n/a | n/a | n/a | n/a |

Notes:

[1] PM₁₀ concentrations are no longer routinely monitored in Ontario. The 90th percentile for PM₁₀ was calculated based on the 90th percentile for PM_{2.5} concentration times a factor of 1.7.

Background concentrations (i.e., concentrations due to natural, nearby, and unidentified sources of all types) are an important part of the total air quality concentration. The dispersion model predicts the incremental impact of the project. Background levels (90th percentile) from this monitoring site for Year 2003 to 2007 are added to the modeled concentrations in determining the worst-case combined impact of the project and the background.

7. METHODOLOGY

The following summarizes the methodology used for the local air quality assessment. This methodology included emission estimates, dispersion modelling, and addition of background concentration. Further details of the methodology for the emission estimates and dispersion modelling are provided in Appendix A.

7.1 Emission Rate Calculations

The emissions from a motor vehicle depend on a large number of factors, including the type, age, and weight of the vehicle, the mode of operation, the weather conditions, and the maintenance condition of the vehicle and of the road. The standard approach for estimating vehicular emissions is to use computer simulation techniques that are based on extensive previous testing of a wide range of vehicles. The most widely used software for this purpose was developed by the U.S. Environmental Protection Agency, and the latest version of the software is known as MOBILE6.2. Key model inputs including climate data and vehicle classification information are provided in Appendix A and discussed in Section 8 of this report.

MOBILE6.2 provides default percentages of each vehicle type. The heavy duty gasoline vehicles (HDGV) and heavy duty diesel vehicles (HDDV) were categorized as heavy-duty vehicle (HDV) and the remaining vehicle types were categorized as light duty vehicles (LDV). AECOM provided a breakdown of LDV and HDV traffic volumes, which were used to calculate composite emission factors for each vehicle type. The resultant emission factors are presented in Appendix A.

MOBILE6.2 was applied to determine average emissions per vehicle under typical winter temperature conditions. The winter condition was chosen to represent worst-case emissions, since vehicle tend to operate less efficiently and produce higher emissions at colder temperatures. Information on how MOBILE6.2 emission factors vary by vehicle speed, temperature, and regulatory changes is given in Appendix A. For both the future build scenario, vehicles were assumed to be operating at the posted speed limits, with no change in average travel speed between scenarios.

In addition to tailpipe emissions, emissions of particulate matter also result from the re-suspension of dust as vehicles travel over a roadway surface. The road dust emissions were calculated based on the U.S. EPA's AP-42, Chapter 13.2.1 emission factors for paved roads. For particulate matter, the tailpipe emission factor is added to the road dust emission factor in order to account for both emission sources. Details of the assumptions applied in the emission estimates are provided in Appendix A.



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7.2 Meteorological Data

Two meteorological datasets are needed in order to perform a dispersion modelling analysis using the CAL3QHCR model: upper air data and surface data. Upper air data were obtained from the Buffalo Airport station (i.e., the nearest upper air measurement site) for the year 2007 and surface data were obtained from Toronto Pearson International Airport for the year 2007. These meteorological datasets were processed using PCRAMMET prior to use with CAL3QHCR.

The choice of meteorological year was based on the results of a screening level analysis of three years of met data (i.e. 2003, 2005 and 2007). This screening level assessment involved running the CAL3HCQR model for a single contaminant using each of the three years of met data, and comparing the results. The analysis indicated that year-to-year variations met conditions and the associated effects on dispersion are relatively small, especially with respect to pollutant concentrations under worst-case meteorological conditions over shorter averaging times (1-hour and 24-hour).

7.3 Dispersion Modelling

Air contaminants emitted from vehicles on a roadway will drift downwind and disperse as they travel. The degree to which the contaminants disperse depends on the weather-related factors, such as wind speed and amount of turbulence. The only approach to determine potential future downwind concentrations from a proposed project is through the use of computer simulation that predicts the dispersal of air pollutants as they drift away from the roads. These simulations are referred to as dispersion models.

Dispersion modelling is a very common approach for assessing local air quality near an emission source such as vehicular traffic. The U.S. EPA developed a model known as CAL3QHCR that is intended specifically to predict air contaminant levels along segmented sections of the roadway, referred to as links. The model takes the emission data and combines it with historical hourly meteorological data, information on traffic volumes, and the configuration of the roadway. It uses this information to predict roadway contributions to air quality levels at selected locations (sensitive receptors) adjacent to the highway under a variety of weather conditions. Appendix A provides a summary of key input parameters.

The CAL3QHCR dispersion model predicts air pollutant concentrations near highways and arterial roads by allocating emissions from motor vehicles to a series of linear emission sources, known as roadway links. A new link must be defined whenever the road width, traffic volume, speed, alignment, or type of traffic movement (free flow or queue) changes. The sections of roadway that were included in the modelling are shown in Figure 1 to Figure 3.

A free flow link is defined as a straight segment of roadway having a constant width, grade height, traffic volume, travel speed, and vehicle emission factor. A queue link is defined as a straight segment of roadway with constant width and emission source strength, on which vehicle idling takes place for specified periods of time (e.g., signalized intersections). The model calculates the contribution from all of the relevant links to each individual receptor so that the cumulative impact can be determined [9,10]. Vehicles were assumed to be traveling at the posted speed limit for each of the roads in the modelled study area. The roadway segments considered in the modelling had speeds of 60 km/hr. A vehicle speed of 4 km/hr was assigned to the queue links, as this is the lowest speed that can be used to calculate tailpipe emissions from the MOBILE6.2 model.

In the context of this air quality assessment, sensitive receptors refer to residences, churches, daycare facilities, hospitals and senior housing facilities throughout the study area. Special consideration is given to sensitive receptors because of the increased potential for adverse health effects at these locations.

A total of 26 receptors were identified within 500 m distance along and in the vicinity of the proposed study area and have been included in the model. Refer to Figures 1 to 3 for the sensitive receptor locations considered in the assessment.



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7.4 Addition of Background Data

The predicted maximum concentrations resulting from the project as well as significant existing arterial roads in the local study area, as predicted by the dispersion model, were added to the 90th percentile background concentrations in order to determine the reasonable worst-case combined (cumulative) effect.

The 90th percentile is the value below which 90% of all monitored data falls. It excludes unusual events at the monitoring stations that are unrepresentative of general background air quality in the area. It is also considered to be the maximum background level that is likely to coincide with worst-case contributions from the modelled sources in the study area. In order to assess attainment, the maximum cumulative concentrations of the contaminants were compared to their applicable ambient thresholds.

7.5 Ozone Limiting Method

When oxides of nitrogen (NO_x) are emitted in diesel exhaust, their initial composition is dominated by nitric oxide (NO). Once in the outside air, some of the NO is oxidized in reactions with other pollutants (principally ground-level ozone) to produce NO_2 , which is a contaminant of concern with established air quality thresholds.

For the purposes of this assessment, the Ozone Limiting Method (OLM) was used to estimate the maximum short-term NO_2 concentrations resulting from emissions of NO_x . This method assumes that the conversion of NO to NO_2 is limited only by the amount of ozone (O_3) present in the outside air. If the concentration of available O_3 (ppm) is less than that of the NO contributed by the modeled roadway emissions, then the portion of NO that is converted to NO_2 equals the available O_3 . On the other hand, if the concentration of available O_3 exceeds that of the NO contributed by the modeled roadway, then all of the NO is converted to NO_2 . The OLM method also assumes that approximately 10% of the emitted NO_x is already in the form of NO_2 before exiting the tailpipe. The OLM is expressed mathematically as follows:

$$\begin{aligned} \text{If } 0.9\text{NO}_x < \text{O}_3, \text{ then } \text{NO}_2 &= \text{NO}_x \\ \text{If } 0.9\text{NO}_x > \text{O}_3, \text{ then } \text{NO}_2 &= 0.1\text{NO}_x + \text{O}_3 \end{aligned}$$

For initial worst-case estimates of cumulative NO_2 concentrations, a fixed concentration of O_3 was used in this calculation. It was set equal to the 90th percentile of measured values from historical monitoring data. For subsequent detailed analysis of cumulative effects, hour-by-hour O_3 data were used.

8. RESULTS

8.1 Assessment of Maximum Credible Impacts

Table 8.1 present a summary of the worst-case predicted combined concentrations (incremental plus background) at the most impacted sensitive receptors. The resultant concentrations are compared to applicable thresholds in order to assess attainment. The predicted concentrations for each contaminant at each sensitive receptor location are provided in Appendix B.

In all cases, the predicted contributions from the modelled roadway are very small compared to the applicable threshold. When added to a representative high background level (the 90th percentile) the combined concentration in all cases is below the threshold. The contaminant that had the highest combined concentration as a percentage of its threshold was PM_{10} , with a percentage of 90%. Therefore, the proposed project is not expected to cause any air contaminant concentrations to exceed their applicable thresholds.



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Table 8.1: Worst-Case Predicted Concentrations ($\mu\text{g}/\text{m}^3$) for the Future-Build Alternative (2031)

| Contaminant | Averaging Period | Most Impacted Receptors | Predicted Concentration ($\mu\text{g}/\text{m}^3$) | 90th Percentile Background ($\mu\text{g}/\text{m}^3$) | Cumulative Concentration ($\mu\text{g}/\text{m}^3$) | Threshold ($\mu\text{g}/\text{m}^3$) | Attainment |
|-------------------|------------------|-------------------------|--|---|---|--|------------|
| CO | 1 hr | R4 | 783 | 836 | 1619 | 36,200 | Yes |
| | 8 hr | R4 | 470 | 502 | 971 | 15,700 | Yes |
| NO ₂ | 1 hr | R4 | 39 | 67 | 106 | 400 | Yes |
| | 24 hr | R4 | 12.2 | 30.4 | 42.6 | 200 | Yes |
| PM _{2.5} | 24 hr | R13 | 1.08 | 18.2 | 19.3 | 30 | Yes |
| PM ₁₀ | 24 hr | R13 | 11.3 | 33.7 | 45.0 | 50 | Yes |

8.2 Concentration Profiles

Concentration profiles illustrate how the maximum predicted 24-hr average concentrations vary with increasing downwind distance away from the roadway. The concentration distance profiles generated for all the pollutants are shown in Figures 4 to 7. For this study, a section of roadway between Hillside Dr. and Hazelwood Dr. was selected, since this is one of the worst-case sections in terms of traffic volumes. The profiles extended 300 m at right angles on either side of the highway, with receptors placed at 20 m intervals. The resulting concentration profiles can be applied to all sections along Dixie Road, as a worst-case representation, to provide an understanding of impacts at locations not explicitly modelled.

The section with the highest traffic volumes was between Queen St. and Hillside Dr., however, it was expected that the similarly higher traffic volumes along Queen St. would have an impact on the receptors in the profile, resulting in a concentration profile which is not representative of the impacts from Dixie Road itself. The section chosen was assumed to be reasonably conservative as the traffic volumes were similar to the actual worst-case section (total traffic volume approximately 2% less than the worst-case).

The concentration profiles illustrate that as the downwind distance from the highway increases, the predicted concentrations decrease. This is expected to occur, since atmospheric dilution of the pollutants increases with distance.

8.3 Discussion of Health Impacts

A qualitative assessment was conducted to evaluate the overall air quality effects as an initial screen for evaluating potential health impacts. The previous sections detail the worst-case predicted concentrations at receptors of varying distance from the roadway (Section 8.2) and comparisons of receptor impacts with the applicable thresholds (Section 8.1). The thresholds adopted for this assessment are effect-based air quality criteria and are set at levels that represent desirable or acceptable levels in ambient air [11]. Ambient concentrations of pollutants less than these criteria are unlikely to represent a significant risk to human health.

From the concentration profiles (Figures 4 to 7) and Table 8.1, it can be seen that concentrations attributable to the roadway are generally much lower than background pollutant concentrations. Importantly, the combined pollutant concentrations for all substances are less than the applicable thresholds for contaminants. Collectively, the results indicate that overall air quality is acceptable and that adverse health impacts are unlikely. A further explanation of the significance of the predicted pollutant concentrations with respect to human health is provided below.

Carbon Monoxide: The results show that the contribution of carbon monoxide across all receptors is on average less than 60% of background levels and the combined concentration is less than 5% of the threshold. The incremental change from existing conditions would be an even smaller percentage. Based on this finding, it was concluded that any incremental increase in CO concentrations due to the widening of Dixie Road is unlikely to result in adverse health impacts.



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Nitrogen Dioxide: The results show that the contribution of nitrogen oxides across all receptors is on average less than 40% of background levels and the combined concentration is less than 26% of the threshold. This level is not only within the MOE's air quality thresholds but also within a lower guideline level, for 1-hour NO_2 of $200 \mu\text{g}/\text{m}^3$, set by the World Health Organization based on a potential for increased bronchial effects in asthmatics [12]. The incremental change from existing conditions would be an even smaller percentage. Based on this finding, it was concluded that any incremental increase in NO_2 concentrations due to the widening of Dixie Road is unlikely to result in adverse health impacts.

PM_{10} : The data show that the combined concentration of PM_{10} at the worst-case receptor is approximately 90% of the threshold. However, the road contributes on average less than 15% of the background levels across all receptors. The incremental change from existing conditions would be an even smaller percentage. While it is possible that there might be a few days after application of road salt or sand for ice control when PM_{10} levels are higher, these would occur during the winter when the background PM_{10} concentrations will be lower. Therefore, the proposed project will not significantly increase the potential for the threshold to be exceeded.

$\text{PM}_{2.5}$: The model results indicate that although the combined concentration of $\text{PM}_{2.5}$ is roughly 64% of the AAQC at a worst-case receptor, the concentration attributable to the highway across all receptors is on average less than 3% of the background. However, as identified above there would be periods of a few days after application of road salt or sand for ice control when the road surface silt loading may be significantly higher, which would contribute to increased $\text{PM}_{2.5}$ concentrations. However, during the winter the background PM concentrations will generally be lower as mentioned.

Recent epidemiological studies indicate that exposure to $\text{PM}_{2.5}$ at concentrations below the threshold may be associated with an increased level of risk in sensitive individuals [13]. The World Health Organization concluded that the low end of the range of $\text{PM}_{2.5}$ concentrations at which health effects have been demonstrated is not much above pristine background levels [12]. However, the project roadway's incremental contribution is so small and localized, that any effect to the population is unlikely to be discernable.

9. CONCLUSIONS

The conclusions of the assessment can be summarized as follows:

- Incremental pollutant concentrations attributable to the roadway are much lower than background pollutant concentrations, and, when combined with representative high background concentrations (90th percentile level), are below the applicable thresholds.
- PM_{10} was the contaminant with the highest percentage of its respective standard.
- The collective results indicate that overall, air quality is acceptable and the potential for unacceptable health impacts due to the project is low.
- Based on the findings, it was concluded that any health impacts associated with emissions from the project would be essentially indistinguishable from those attributable to normal background.



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FIGURES



LEGEND:
 Roadway Link
 Discrete Receptor

Site Plan Showing Location of Roadway Links and Discrete Receptors
 2km North of Mayfield Road to Mayfield Road

Drawn by: NTN Figure: 1
 Approx. Scale: 1:10,000
 Date Revised: Nov 26, 2010

True North

Project: m925103
 Draw: Rd.Wildemup EA - Pres Region, Ontario

RWDI



LEGEND:
 Roadway Link
 Discrete Receptor

Site Plan Showing Location of Roadway Links and Discrete Receptors
 Mayfield Road to Peter Robertson Boulevard

Drawn by: NTN Figure: 2
 Approx. Scale: 1:10 000
 Date Revised: June 10, 2009
 Project m925103

RWDI

Dixie Rd/Walton Rd - Peel Region, Ontario



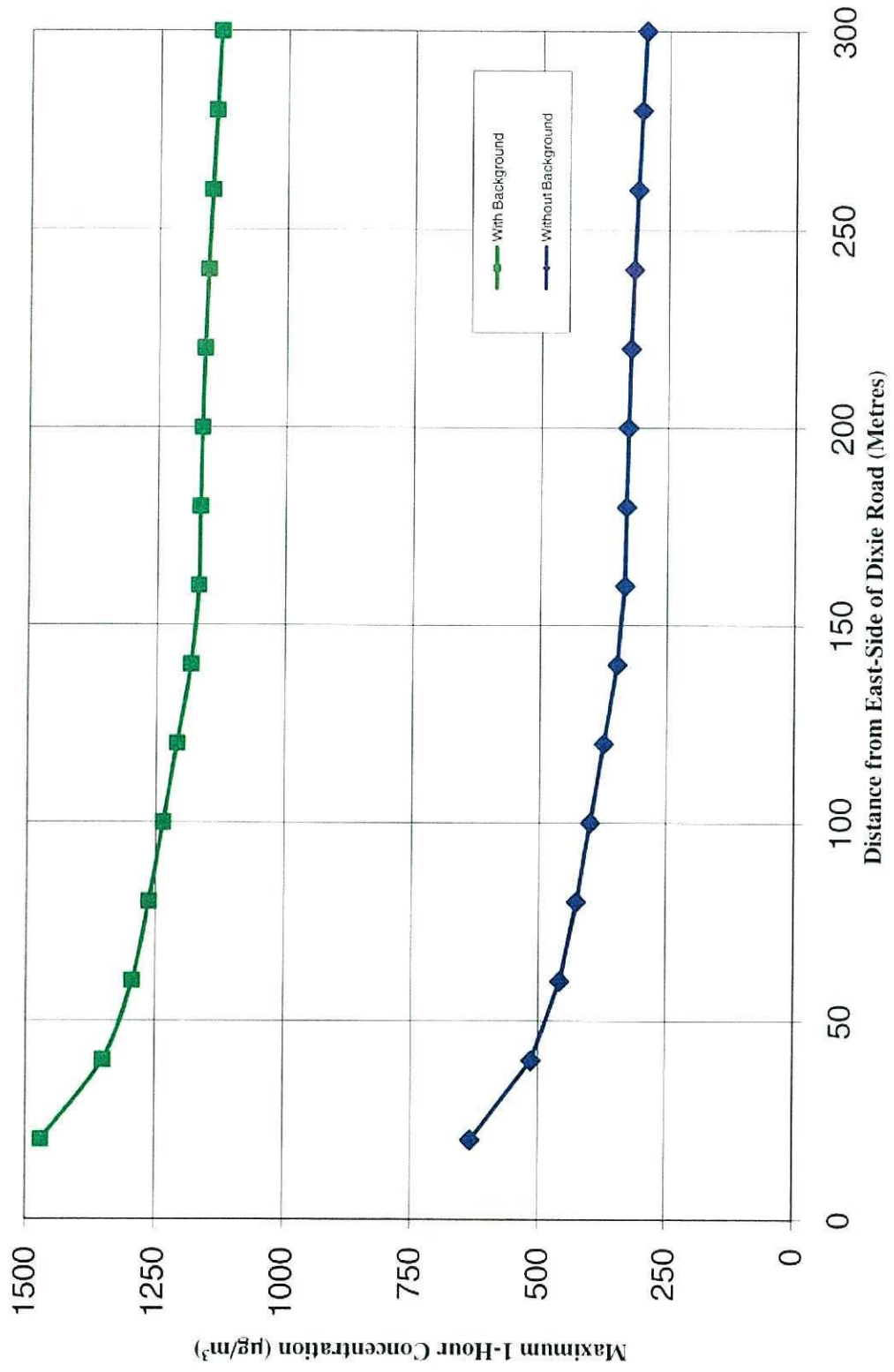
Title: **Site Plan Showing Location of Roadway Links and Discrete Receptors**
 Project: **Peter Robertsen Boulevard in Queen Street East**
 Drawn by: **NTN** Figure: **3**
 Approx. Scale: **1:10,000**
 Date Revised: **June 10, 2009**
 Project: **mp251p1**
 Drawn by: **RD Walden, E.A.** Peer Review: **Onsite**



RWDI
 Project: **mp251p1**
 Date Revised: **June 10, 2009**

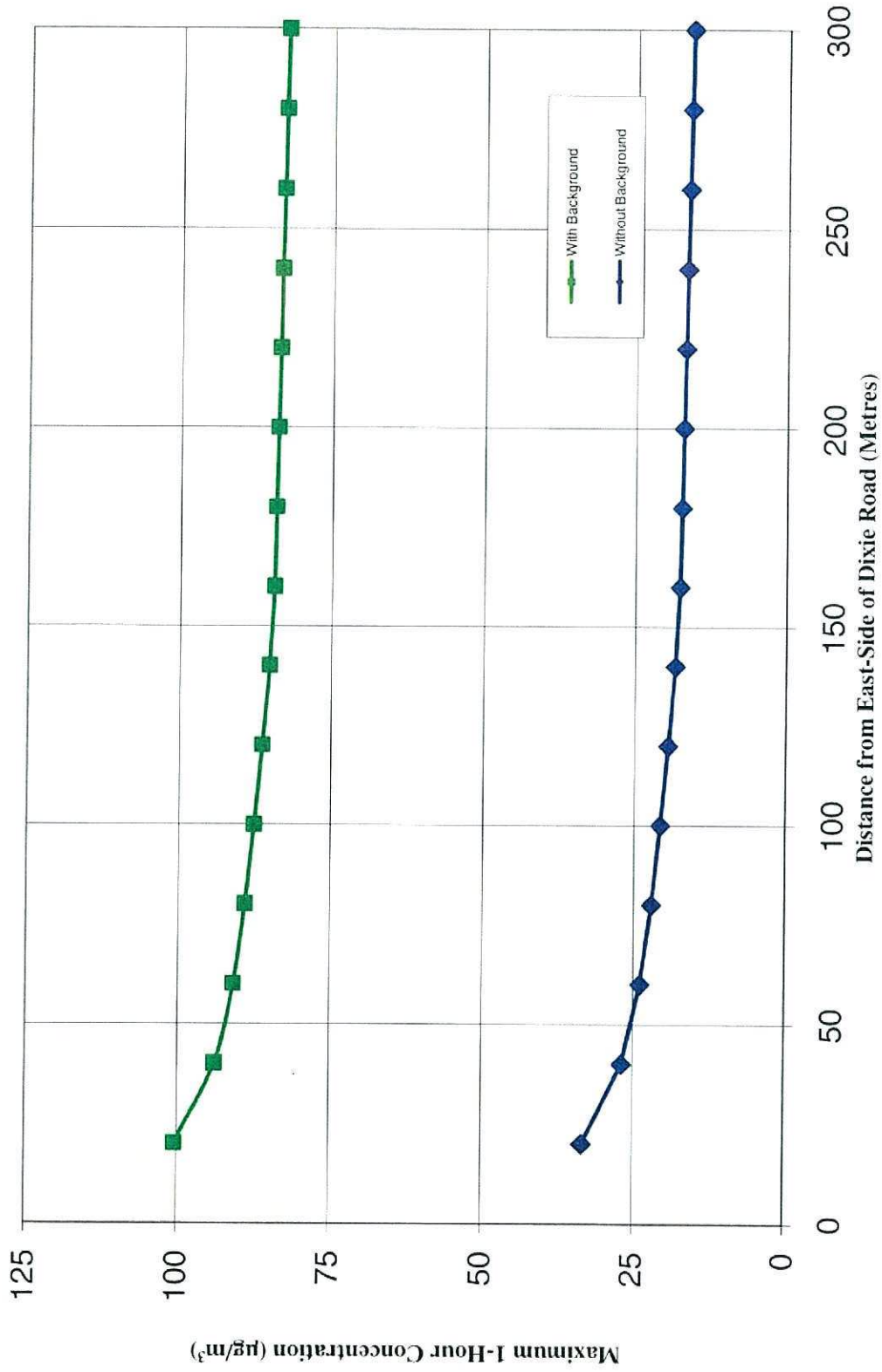
LEGEND
 Roadway Link
 Discrete Receptor

Figure 4: Concentration Profile for CO
 Year 2031 Future Build



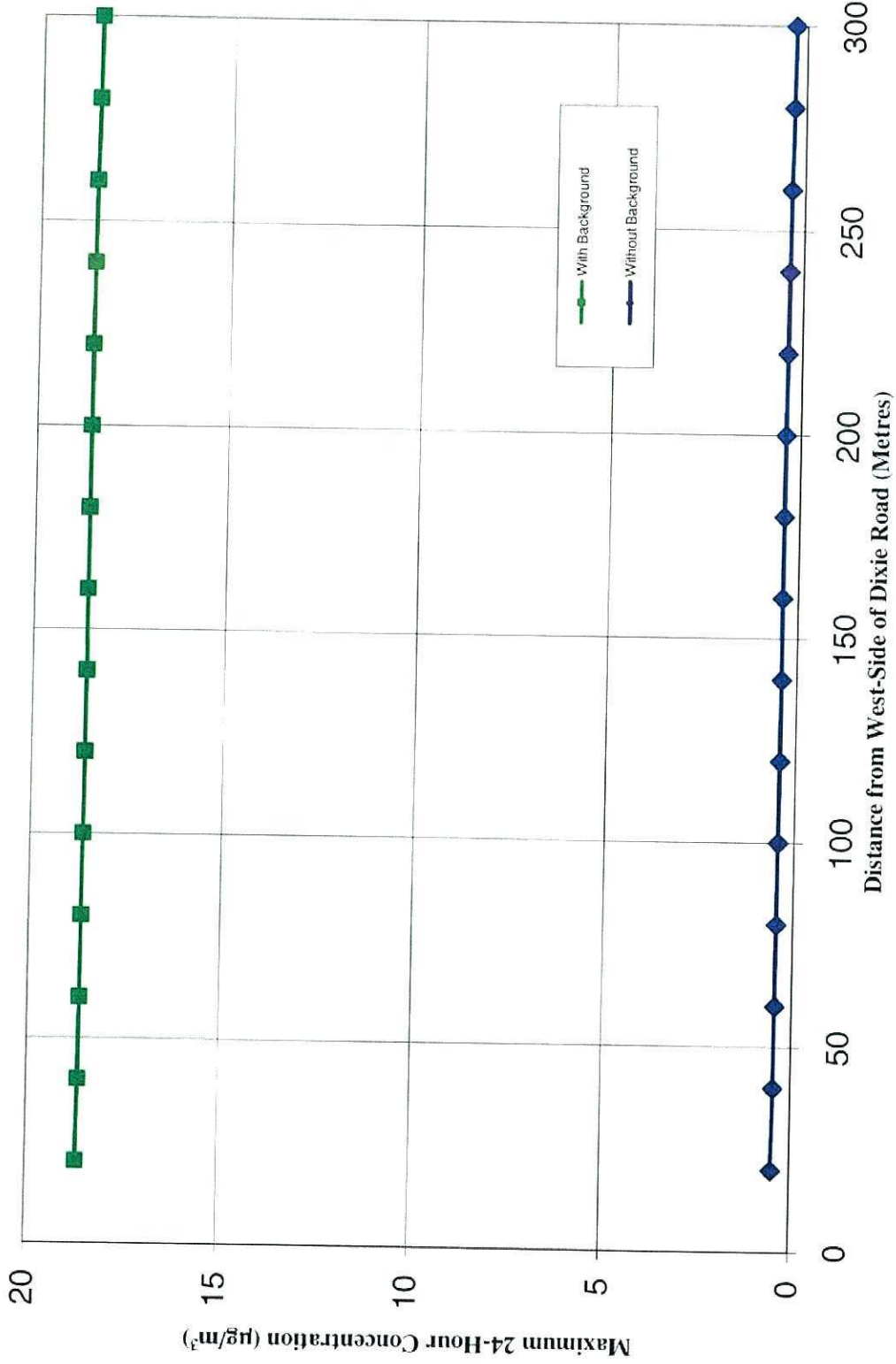
Note: MOE's 24-hr AAQC for CO is 36,200 $\mu\text{g}/\text{m}^3$
 The 90th percentile is 836 $\mu\text{g}/\text{m}^3$ (2005 - 2 007 - Toronto West MOE Station 35 125, 2003-2004 - Brampton MOE Station 46089).

Figure 5: Concentration Profile for NO₂
 Year 2031 Future Build



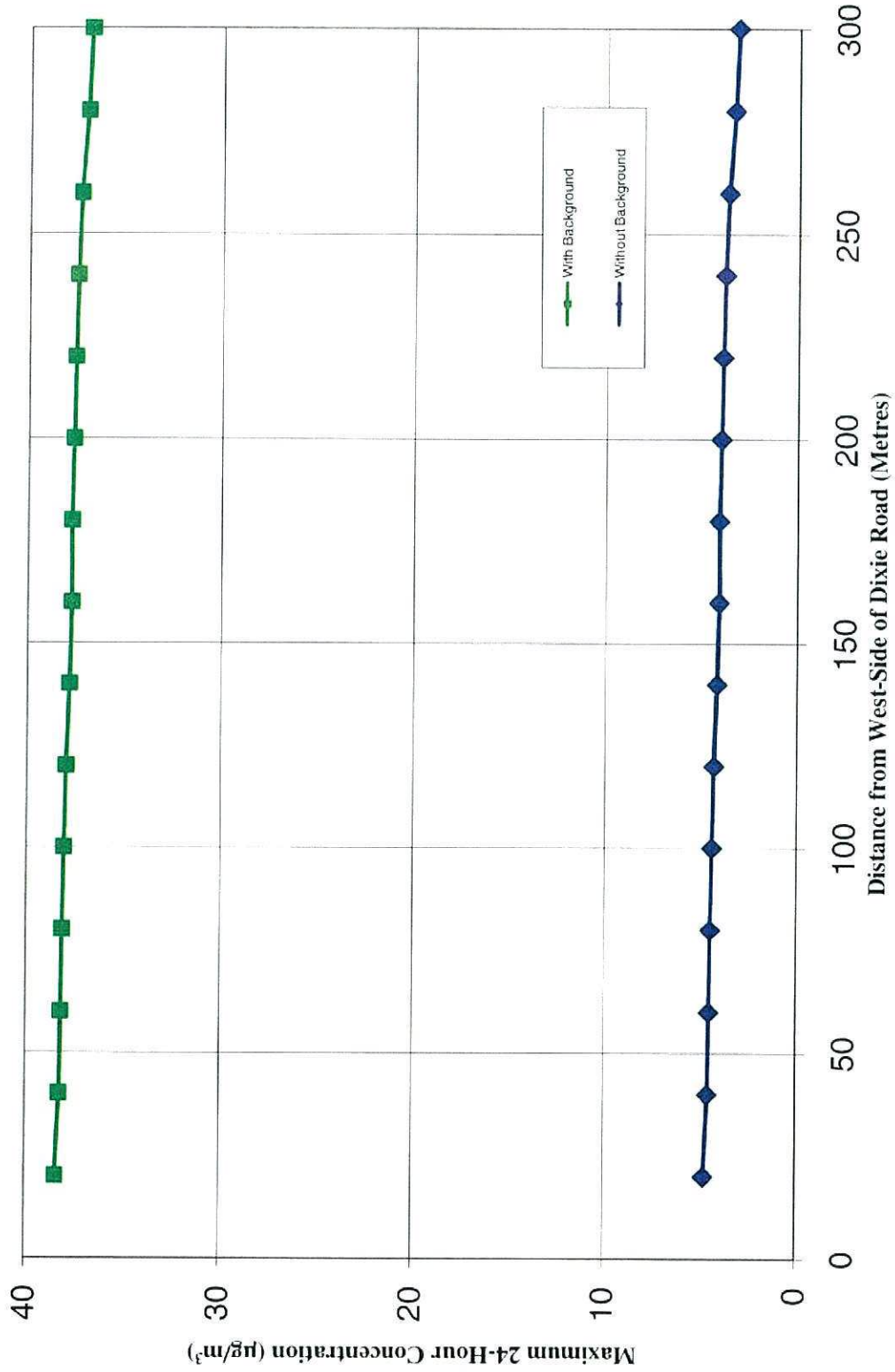
Note: MOE's 24-hr AAQC for NO₂ is 400 µg/m³
 The 90th percentile from 2003-2007 is 67 µg/m³ (Brampton: MOE 46089).

Figure 6: Concentration Profile for PM_{2.5}
 Year 2031 Future Build



Note: Canada Wide Standard for PM_{2.5} is 30 µg/m³
 The 90th percentile from 2003-2007 is 18.2 µg/m³ (Brampton, MOE 46089)

Figure 7: Concentration Profile for PM₁₀
 Year 2031 Future Build



Note: MOE's 24-hr AAQC for PM₁₀ is 50 µg/m³
 The 90th percentile from 2003-2007 is 33.7 µg/m³ (Brampton, MOE-46089).

APPENDIX A

Table A1: MOBILE6.2 Key Model Input Parameters [1]

| Parameter | Input |
|---------------------|--|
| Pollutants | CO, NO _x , PM ₁₀ , and PM _{2.5} . |
| Operating Year | 2031 |
| Evaluation Month | January |
| Ambient Temperature | Minimum Daily Temperature = 13.1 °F (-10.5 °C) Maximum Daily Temperature = 28.2 °F (-2.1 °C) (Canadian Climate Normals, Toronto Lester B. Pearson International Airport Station) |
| Altitude | Low |
| Absolute Humidity | 20 Grains /lb |
| Fuel Volatility | Reid Vapor Pressure (RVP) = 9 psi |
| Fuel Program | Conventional Gasoline East |
| Vehicle Speed | 60 km/hr and 4 km/hr |

Note: [1] The idle condition is represented by a speed of 4km/hr since this is the lowest speed MOBILE6.2 can model

Table A2: MOBILE6.2 Vehicle Classification System [1]

| Vehicle Class | Description |
|---------------|--|
| LDGV | Light-Duty Gas Vehicles (Passenger Cars) |
| LDGT1 | Light-Duty Gas Trucks 1 (0-6,000 lbs. GVWR, 0-3,750 lbs LVW) |
| LDGT2 | Light-Duty Gas Trucks 2 (0-6,000 lbs GVWR, 3,751-5,750 lbs LVW) |
| LDGT3 | Light-Duty Gas Trucks 3 (6,001-8,500 lbs GVWR, 0-5,750 lbs ALVW) |
| LDGT4 | Light-Duty Gas Trucks 4 (6,001-8,500 lbs GVWR, > 5,750 lbs ALVW) |
| HdGV2b | Class 2b Heavy-Duty Gasoline Vehicles (8,501-10,000 lbs GVWR) |
| HdGV3 | Class 3 Heavy-Duty Gasoline Vehicles (10,001-14,000 lbs GVWR) |
| HdGV4 | Class 4 Heavy-Duty Gasoline Vehicles (14,001-16,000 lbs GVWR) |
| HdGV5 | Class 5 Heavy-Duty Gasoline Vehicles (16,001-19,500 lbs GVWR) |
| HdGV6 | Class 6 Heavy-Duty Gasoline Vehicles (19,501-26,000 lbs GVWR) |
| HdGV7 | Class 7 Heavy-Duty Gasoline Vehicles (26,001-33,000 lbs GVWR) |
| HdGV8a | Class 8a Heavy-Duty Gasoline Vehicles (33,001-60,000 lbs GVWR) |
| HdGV8b | Class 8b Heavy-Duty Gasoline Vehicles (>60,000 lbs GVWR) |
| LDDV | Light-Duty Diesel Vehicles (Passenger Cars) |
| LDDT12 | Light-Duty Diesel Trucks 1 and 2 (0-6,000 lbs GVWR) |
| HDDV2b | Class 2b Heavy-Duty Diesel Vehicles (8,501-10,000 lbs GVWR) |
| HDDV3 | Class 3 Heavy-Duty Diesel Vehicles (10,001-14,000 lbs GVWR) |
| HDDV4 | Class 4 Heavy-Duty Diesel Vehicles (14,001-16,000 lbs GVWR) |
| HDDV5 | Class 5 Heavy-Duty Diesel Vehicles (16,001-19,500 lbs GVWR) |
| HDDV6 | Class 6 Heavy-Duty Diesel Vehicles (19,501-26,000 lbs GVWR) |
| HDDV7 | Class 7 Heavy-Duty Diesel Vehicles (26,001-33,000 lbs GVWR) |
| HDDV8a | Class 8a Heavy-Duty Diesel Vehicles (33,001-60,000 lbs GVWR) |
| HDDV8b | Class 8b Heavy-Duty Diesel Vehicles (>60,000 lbs GVWR) |
| MC | Motorcycles (Gasoline) |
| HDGB | Gasoline Buses (School, Transit and Urban) |
| HDDBT | Diesel Transit and Urban Buses |
| HDDBS | Diesel School Buses |
| LDDT34 | Light-Duty Diesel Trucks 3 and 4 (6,001-8,500 lbs GVWR) |

Notes: GVWR – Gross vehicle weight rating
LVW – Loaded vehicle weight

Table A3.1: Summary of LDV Emission Factors from MOBILE6.2 (g/VMT)

| Year | Pollutant | 60 km/h | 4 km/hr |
|------|----------------------------------|---------|---------|
| 2031 | CO | 6.51 | 27.4 |
| | NO _x | 0.35 | 0.73 |
| | PM ₁₀ ^[1] | 0.02 | 0.02 |
| | PM _{2.5} ^[1] | 0.01 | 0.01 |

Notes: VMT – Vehicle miles traveled
 [1] MOBILE6.2 particulate matter emission factors are not speed dependant.
 Vehicle particulate matter emission factors include exhaust, brake wear, and tire wear

Table A3.2: Summary of HDV Emission Factors from MOBILE6.2 (g/VMT)

| Year | Pollutant | 60 km/h | 4 km/hr |
|------|----------------------------------|---------|---------|
| 2031 | CO | 2.10 | 13.8 |
| | NO _x | 0.39 | 0.70 |
| | PM ₁₀ ^[1] | 0.05 | 0.05 |
| | PM _{2.5} ^[1] | 0.03 | 0.03 |

Notes: VMT – Vehicle miles traveled
 [1] MOBILE6.2 particulate matter emission factors are not speed dependant.
 Vehicle particulate matter emission factors include exhaust, brake wear, and tire wear

Table A4: Summary of AP-42 Re-entrained Road Dust Emission Factors

| | k (g/VMT) |
|-------|-----------|
| PM2.5 | 1.1 |
| PM10 | 7.3 |

| Index | Scenario | ADT Category | sL (g/m2) | LDV W (tons) | HDV W (tons) | Percent HDV | Average W (tons) | PM2.5 (with 80s Tailpipe) | PM10 (with 80s Tailpipe) | Re-Entrained PM2.5 (80s Tailpipe Removed) | Re-Entrained PM10 (80s Tailpipe Removed) |
|-------|--------------------------------|--------------|-----------|--------------|--------------|-------------|------------------|---------------------------|--------------------------|---|--|
| 1 | Scenario 1 (0% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 0% | 1.9 | 0.6242 | 4.1423 | 0.4625 | 3.9304 |
| 2 | Scenario 2 (0% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 0% | 1.9 | 0.2555 | 1.6823 | 0.0918 | 1.4704 |
| 3 | Scenario 3 (0% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 0% | 1.9 | 0.0891 | 0.5910 | 0.0000 | 0.3791 |
| 4 | Scenario 4 (0% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 0% | 1.9 | 0.0362 | 0.2400 | 0.0000 | 0.0281 |
| 5 | Scenario 5 (1% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 1% | 2.1 | 0.2841 | 1.6854 | 0.1224 | 1.6735 |
| 6 | Scenario 6 (1% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 1% | 2.1 | 0.0998 | 0.6623 | 0.0000 | 0.4504 |
| 7 | Scenario 7 (1% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 1% | 2.1 | 0.0998 | 0.6623 | 0.0000 | 0.4504 |
| 8 | Scenario 8 (1% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 1% | 2.1 | 0.0405 | 0.2690 | 0.0000 | 0.0571 |
| 9 | Scenario 9 (2% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 2% | 2.2 | 0.7777 | 5.1611 | 0.6160 | 4.9492 |
| 10 | Scenario 10 (2% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 2% | 2.2 | 0.3158 | 2.0961 | 0.1541 | 1.8842 |
| 11 | Scenario 11 (2% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 2% | 2.2 | 0.1110 | 0.7363 | 0.0000 | 0.5244 |
| 12 | Scenario 12 (2% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 2% | 2.2 | 0.0451 | 0.2990 | 0.0000 | 0.0871 |
| 13 | Scenario 13 (3% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 3% | 2.4 | 0.8586 | 5.6978 | 0.6969 | 5.4859 |
| 14 | Scenario 14 (3% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 3% | 2.4 | 0.3467 | 2.3140 | 0.1870 | 2.1021 |
| 15 | Scenario 15 (3% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 3% | 2.4 | 0.1225 | 0.8129 | 0.0000 | 0.6010 |
| 16 | Scenario 16 (3% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 3% | 2.4 | 0.0497 | 0.3301 | 0.0000 | 0.1182 |
| 17 | Scenario 17 (4% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 4% | 2.5 | 0.3826 | 2.5391 | 0.2209 | 2.3272 |
| 18 | Scenario 18 (4% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 4% | 2.5 | 0.1344 | 0.8920 | 0.0000 | 0.6801 |
| 19 | Scenario 19 (4% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 4% | 2.5 | 0.0546 | 0.3623 | 0.0000 | 0.1504 |
| 20 | Scenario 20 (5% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 5% | 2.7 | 1.0281 | 6.8230 | 0.8664 | 6.6111 |
| 21 | Scenario 21 (5% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 5% | 2.7 | 0.4175 | 2.7710 | 0.2558 | 2.5591 |
| 22 | Scenario 22 (5% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 5% | 2.7 | 0.1467 | 0.9734 | 0.0000 | 0.7615 |
| 23 | Scenario 23 (5% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 5% | 2.7 | 0.0506 | 0.3953 | 0.0000 | 0.1834 |
| 24 | Scenario 24 (6% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 6% | 2.8 | 0.4535 | 3.0396 | 0.2918 | 2.7977 |
| 25 | Scenario 25 (6% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 6% | 2.8 | 0.1593 | 1.0572 | 0.0000 | 0.8453 |
| 26 | Scenario 26 (6% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 6% | 2.8 | 0.0647 | 0.4294 | 0.0000 | 0.2175 |
| 27 | Scenario 27 (7% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 7% | 3.0 | 1.2076 | 8.0139 | 1.0459 | 7.8020 |
| 28 | Scenario 28 (7% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 7% | 3.0 | 0.4904 | 3.2546 | 0.3287 | 3.0427 |
| 29 | Scenario 29 (7% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 7% | 3.0 | 0.1723 | 1.1433 | 0.0106 | 0.9314 |
| 30 | Scenario 30 (7% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 7% | 3.0 | 0.0700 | 0.4643 | 0.0000 | 0.2524 |
| 31 | Scenario 31 (8% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 8% | 3.1 | 0.5293 | 3.5060 | 0.3666 | 3.2941 |
| 32 | Scenario 32 (8% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 8% | 3.1 | 0.0754 | 0.5002 | 0.0000 | 0.2883 |
| 33 | Scenario 33 (9% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 9% | 3.3 | 0.5671 | 3.7635 | 0.4054 | 3.5516 |
| 34 | Scenario 34 (10% HDV) | < 500 | 2.4 | 1.9 | 16.9 | 10% | 3.4 | 1.4942 | 9.9158 | 1.3325 | 9.7039 |
| 35 | Scenario 35 (10% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 10% | 3.4 | 0.6068 | 4.0271 | 0.4451 | 3.8152 |
| 36 | Scenario 36 (10% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 10% | 3.4 | 0.2132 | 1.4147 | 0.0515 | 1.2028 |
| 37 | Scenario 37 (10% HDV) | > 10,000 | 0.03 | 1.9 | 16.9 | 10% | 3.4 | 0.0866 | 0.5745 | 0.0000 | 0.3628 |
| 38 | Scenario 38 (11% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 11% | 3.6 | 0.6474 | 4.2965 | 0.4857 | 4.0846 |
| 39 | Scenario 39 (12% HDV) | < 10,000 | 0.12 | 1.9 | 16.9 | 12% | 3.7 | 0.2420 | 1.6060 | 0.0803 | 1.3941 |
| 40 | Scenario 40 (12% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 12% | 3.7 | 0.6889 | 4.5716 | 0.5272 | 4.3597 |
| 41 | Scenario 41 (13% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 13% | 3.9 | 0.7312 | 4.8524 | 0.5695 | 4.6405 |
| 42 | Scenario 42 (16% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 16% | 4.3 | 0.8631 | 5.7276 | 0.7014 | 5.5157 |
| 43 | Scenario 43 (17% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 17% | 4.5 | 0.9086 | 6.0299 | 0.7469 | 5.8180 |
| 44 | Scenario 44 (18% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 18% | 4.6 | 0.9549 | 6.3373 | 0.7932 | 6.1254 |
| 45 | Scenario 45 (22% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 22% | 5.2 | 1.1477 | 7.8168 | 0.9860 | 7.4049 |
| 46 | Scenario 46 (23% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 23% | 5.4 | 1.1978 | 7.9488 | 1.0361 | 7.7369 |
| 47 | Scenario 47 (29% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 29% | 6.3 | 1.5124 | 10.0367 | 1.3507 | 9.8248 |
| 48 | Scenario 48 (33% HDV) | < 5,000 | 0.6 | 1.9 | 16.9 | 33% | 6.9 | 1.7353 | 11.5161 | 1.5736 | 11.3042 |
| N/A | C - Exhaust, Brake & Tire Wear | n/a | n/a | n/a | n/a | n/a | n/a | 0.1617 | 0.2119 | n/a | n/a |

Notes

1. Re-entrained road dust emission rates are calculated based on equation 1 of AP-42 draft report for paved road emissions (Section 13.2.1)

Table A5: CAL3QHCR Key Input Parameters

| Parameter | Input |
|---|---|
| Meteorological Data | Year 2007 hourly surface data and upper air data are from the Toronto Lester B. Pearson International Airport (12345) and Greater Buffalo International Airport in New York (14733) |
| Traffic Volumes (AADT) | Provided by AECOM |
| Hourly Traffic Volume Distribution | AECOM provided hourly traffic volume distribution for a 24-hour period. |
| Volume of Heavy-Duty Vehicles (HDV) | Provided by AECOM |
| Light Cycle Timing | Provided by AECOM |
| Deposition Velocity | PM ₁₀ = 1.1 cm/s PM _{2.5} = 0.1 cm/s |
| Settling Velocity | PM ₁₀ = 0.5 cm/s PM _{2.5} = 0.005 cm/s |
| Surface Roughness | 108 cm – single family residential |
| Dispersion Coefficient (Urban or Rural) | Urban |

APPENDIX B

APPENDIX B: Tabular Results

Table B.1: Predicted 24-Hour Average PM₁₀ Concentrations, Including 90th Percentile Background Concentration (µg/m³)

| Receptor No. | Predicted Concentration from Dixie Road (µg/m ³) | Future Build Predicted Cumulative Concentration (µg/m ³) [1] | MOE's Interim 24-Hour AAQC(µg/m ³) [2] | Percentage of Guideline Limit (%) |
|--------------|--|--|--|-----------------------------------|
| R1 | 5.4 | 39.1 | 50 | 78% |
| R2 | 2.6 | 36.3 | 50 | 73% |
| R3 | 9.2 | 42.9 | 50 | 86% |
| R4 | 7.6 | 41.3 | 50 | 83% |
| R5 | 4.4 | 38.1 | 50 | 76% |
| R6 | 7.1 | 40.8 | 50 | 82% |
| R7 | 8.8 | 42.5 | 50 | 85% |
| R8 | 5.1 | 38.8 | 50 | 78% |
| R9 | 6.1 | 39.8 | 50 | 80% |
| R10 | 4.8 | 38.5 | 50 | 77% |
| R11 | 4.5 | 38.2 | 50 | 76% |
| R12 | 4.1 | 37.8 | 50 | 76% |
| R13 | 11.3 | 45.0 | 50 | 90% |
| R14 | 3.8 | 37.5 | 50 | 75% |
| R15 | 4.7 | 38.4 | 50 | 77% |
| R16 | 4.6 | 38.3 | 50 | 77% |
| R17 | 3.6 | 37.3 | 50 | 75% |
| R18 | 4.9 | 38.6 | 50 | 77% |
| R19 | 6.9 | 40.6 | 50 | 81% |
| R20 | 4.1 | 37.8 | 50 | 76% |
| R21 | 5.7 | 39.4 | 50 | 79% |
| R22 | 2.3 | 36.0 | 50 | 72% |
| R23 | 2.2 | 35.9 | 50 | 72% |
| R24 | 1.2 | 34.9 | 50 | 70% |
| R25 | 1.8 | 35.5 | 50 | 71% |
| R26 | 0.93 | 34.6 | 50 | 69% |

Notes: [1] Background concentration data not available for PM₁₀, data calculated from PM_{2.5} data.
 [2] The MOE's Interim 24-Hour AAQC for PM₁₀ is 50µg/m³.

Table B.2: Predicted 24-Hour Average PM_{2.5} Concentrations, Including 90th Percentile Background Concentration (µg/m³)

| Receptor No. | Predicted Concentration from Dixie Road (µg/m ³) | Future Build Predicted Cumulative Concentration (µg/m ³) [1] | MOE's Interim 24-Hour AAQC(µg/m ³) [2] | Percentage of Guideline Limit (%) |
|--------------|--|--|--|-----------------------------------|
| R1 | 0.33 | 18.5 | 30 | 62% |
| R2 | 0.20 | 18.4 | 30 | 61% |
| R3 | 1.05 | 19.3 | 30 | 64% |
| R4 | 0.82 | 19.0 | 30 | 63% |
| R5 | 0.35 | 18.6 | 30 | 62% |
| R6 | 0.57 | 18.8 | 30 | 63% |
| R7 | 0.80 | 19.0 | 30 | 63% |
| R8 | 0.38 | 18.6 | 30 | 62% |
| R9 | 0.41 | 18.6 | 30 | 62% |
| R10 | 0.44 | 18.6 | 30 | 62% |
| R11 | 0.46 | 18.7 | 30 | 62% |
| R12 | 0.42 | 18.6 | 30 | 62% |
| R13 | 1.08 | 19.3 | 30 | 64% |
| R14 | 0.38 | 18.6 | 30 | 62% |
| R15 | 0.44 | 18.6 | 30 | 62% |
| R16 | 0.41 | 18.6 | 30 | 62% |
| R17 | 0.26 | 18.5 | 30 | 62% |
| R18 | 0.38 | 18.6 | 30 | 62% |
| R19 | 0.67 | 18.9 | 30 | 63% |
| R20 | 0.35 | 18.6 | 30 | 62% |
| R21 | 0.43 | 18.6 | 30 | 62% |
| R22 | 0.17 | 18.4 | 30 | 61% |
| R23 | 0.19 | 18.4 | 30 | 61% |
| R24 | 0.098 | 18.3 | 30 | 61% |
| R25 | 0.18 | 18.4 | 30 | 61% |
| R26 | 0.090 | 18.3 | 30 | 61% |

Notes: [1] The 90th percentile background concentration is from the years 2003-2007 from MOE Station No. 46089 (Brampton).

[2] Canada Wide Standard (CWS) for PM_{2.5} is 30 µg/m³ established for the year 2010 based on the 98th percentile ambient measurement annually, average over three consecutive years.

Table B.3: Predicted 1-Hour Average CO Concentrations, Including 90th Percentile Background Concentration ($\mu\text{g}/\text{m}^3$)

| Receptor No. | Predicted Concentration from Dixie Road ($\mu\text{g}/\text{m}^3$) | Future Build Predicted Cumulative Concentration ($\mu\text{g}/\text{m}^3$) [1] | MOE's 1-Hour AAQC [2] | Percentage of Guideline Limit (%) |
|--------------|--|--|-----------------------|-----------------------------------|
| R1 | 495 | 1,331 | 36,200 | 4% |
| R2 | 438 | 1,274 | 36,200 | 4% |
| R3 | 436 | 1,272 | 36,200 | 4% |
| R4 | 783 | 1,619 | 36,200 | 4% |
| R5 | 452 | 1,288 | 36,200 | 4% |
| R6 | 440 | 1,276 | 36,200 | 4% |
| R7 | 701 | 1,537 | 36,200 | 4% |
| R8 | 501 | 1,337 | 36,200 | 4% |
| R9 | 453 | 1,289 | 36,200 | 4% |
| R10 | 476 | 1,312 | 36,200 | 4% |
| R11 | 696 | 1,532 | 36,200 | 4% |
| R12 | 375 | 1,211 | 36,200 | 4% |
| R13 | 497 | 1,333 | 36,200 | 3% |
| R14 | 428 | 1,264 | 36,200 | 4% |
| R15 | 354 | 1,190 | 36,200 | 3% |
| R16 | 599 | 1,435 | 36,200 | 3% |
| R17 | 343 | 1,179 | 36,200 | 4% |
| R18 | 374 | 1,210 | 36,200 | 3% |
| R19 | 681 | 1,517 | 36,200 | 3% |
| R20 | 280 | 1,116 | 36,200 | 4% |
| R21 | 569 | 1,405 | 36,200 | 3% |
| R22 | 311 | 1,147 | 36,200 | 4% |
| R23 | 388 | 1,224 | 36,200 | 3% |
| R24 | 266 | 1,102 | 36,200 | 3% |
| R25 | 413 | 1,249 | 36,200 | 3% |
| R26 | 277 | 1,113 | 36,200 | 3% |

Notes: [1] The 90th percentile background concentration data from the years 2005-2007 are from MOE Station No. 35125 (Toronto West). Data for the years 2003-2004 are from MOE Station No. 46089 (Brampton).
 [2] The MOE's 1-Hour AAQC for CO is 36,200 $\mu\text{g}/\text{m}^3$.

Table B.4: Predicted 8-Hour Average CO Concentrations, Including 90th Percentile Background Concentration ($\mu\text{g}/\text{m}^3$)

| Receptor No. | Predicted Concentration from Dixie Road ($\mu\text{g}/\text{m}^3$) [1] | Future Build Predicted Cumulative Concentration ($\mu\text{g}/\text{m}^3$) [1][2] | MOE's 1-Hour AAQC [3] | Percentage of Guideline Limit (%) |
|--------------|--|---|-----------------------|-----------------------------------|
| R1 | 297 | 799 | 15,700 | 5% |
| R2 | 263 | 764 | 15,700 | 5% |
| R3 | 261 | 763 | 15,700 | 5% |
| R4 | 470 | 971 | 15,700 | 6% |
| R5 | 271 | 773 | 15,700 | 5% |
| R6 | 264 | 766 | 15,700 | 5% |
| R7 | 421 | 922 | 15,700 | 6% |
| R8 | 301 | 802 | 15,700 | 5% |
| R9 | 272 | 773 | 15,700 | 5% |
| R10 | 286 | 787 | 15,700 | 5% |
| R11 | 418 | 919 | 15,700 | 6% |
| R12 | 225 | 727 | 15,700 | 5% |
| R13 | 298 | 800 | 15,700 | 5% |
| R14 | 257 | 758 | 15,700 | 5% |
| R15 | 213 | 714 | 15,700 | 5% |
| R16 | 359 | 861 | 15,700 | 5% |
| R17 | 206 | 708 | 15,700 | 5% |
| R18 | 224 | 726 | 15,700 | 5% |
| R19 | 409 | 910 | 15,700 | 6% |
| R20 | 168 | 669 | 15,700 | 4% |
| R21 | 342 | 843 | 15,700 | 5% |
| R22 | 187 | 688 | 15,700 | 4% |
| R23 | 233 | 734 | 15,700 | 5% |
| R24 | 160 | 661 | 15,700 | 4% |
| R25 | 248 | 749 | 15,700 | 5% |
| R26 | 166 | 668 | 15,700 | 4% |

Notes: [1] Predicted concentrations and background concentration data was scaled from 1-hour to 8-hour using a 0.6 conversion factor.
 [1] The 90th percentile background concentration data from the years 2005-2007 are from MOE Station No. 35125 (Toronto West). Data for the years 2003-2004 are from MOE Station No. 46089 (Brampton).
 [2] The MOE's 8-Hour AAQC for CO is 15,700 $\mu\text{g}/\text{m}^3$.

Table B.5: Maximum Predicted 1-Hour Average NO₂ Concentrations, Including 90th Percentile Background Concentration (µg/m³)

| Receptor No. | Predicted Concentration from Dixie Road (µg/m ³) | Future Build Predicted Cumulative Concentration (µg/m ³) [1] | MOE's 1-Hour AAQC [2] | Percentage of Guideline Limit (%) |
|--------------|--|--|-----------------------|-----------------------------------|
| R1 | 26 | 93 | 400 | 23% |
| R2 | 24 | 91 | 400 | 23% |
| R3 | 24 | 91 | 400 | 23% |
| R4 | 39 | 106 | 400 | 26% |
| R5 | 24 | 91 | 400 | 23% |
| R6 | 23 | 90 | 400 | 22% |
| R7 | 37 | 104 | 400 | 26% |
| R8 | 26 | 93 | 400 | 23% |
| R9 | 24 | 91 | 400 | 23% |
| R10 | 25 | 92 | 400 | 23% |
| R11 | 36 | 103 | 400 | 26% |
| R12 | 20 | 87 | 400 | 22% |
| R13 | 26 | 93 | 400 | 23% |
| R14 | 23 | 90 | 400 | 22% |
| R15 | 18 | 85 | 400 | 21% |
| R16 | 31 | 98 | 400 | 24% |
| R17 | 18 | 85 | 400 | 21% |
| R18 | 20 | 87 | 400 | 22% |
| R19 | 36 | 103 | 400 | 26% |
| R20 | 15 | 82 | 400 | 21% |
| R21 | 30 | 97 | 400 | 24% |
| R22 | 17 | 84 | 400 | 21% |
| R23 | 21 | 88 | 400 | 22% |
| R24 | 15 | 82 | 400 | 20% |
| R25 | 23 | 90 | 400 | 22% |
| R26 | 15 | 82 | 400 | 21% |

Notes: [1] The 90th percentile background concentration is from the years 2003-2007 from MOE Station No. 46089 (Brampton).

[2] The MOE's 1-Hour AAQC for NO_x is 400µg/m³.

Table B.6: Maximum Predicted 24-Hour Average NO₂ Concentrations, Including 90th Percentile Background Concentration (µg/m³)

| Receptor No. | Predicted Concentration from Dixie Road (µg/m ³) | Future Build Predicted Cumulative Concentration (µg/m ³) [1] | MOE's 1-Hour AAQC [2] | Percentage of Guideline Limit (%) |
|--------------|--|--|-----------------------|-----------------------------------|
| R1 | 7 | 38 | 200 | 19% |
| R2 | 5 | 36 | 200 | 18% |
| R3 | 5 | 36 | 200 | 18% |
| R4 | 12 | 43 | 200 | 21% |
| R5 | 6 | 36 | 200 | 18% |
| R6 | 6 | 36 | 200 | 18% |
| R7 | 11 | 41 | 200 | 21% |
| R8 | 6 | 36 | 200 | 18% |
| R9 | 7 | 37 | 200 | 18% |
| R10 | 6 | 36 | 200 | 18% |
| R11 | 10 | 41 | 200 | 20% |
| R12 | 4 | 35 | 200 | 17% |
| R13 | 7 | 37 | 200 | 19% |
| R14 | 6 | 36 | 200 | 18% |
| R15 | 5 | 35 | 200 | 18% |
| R16 | 8 | 38 | 200 | 19% |
| R17 | 4 | 34 | 200 | 17% |
| R18 | 5 | 35 | 200 | 18% |
| R19 | 9 | 40 | 200 | 20% |
| R20 | 3 | 34 | 200 | 17% |
| R21 | 7 | 38 | 200 | 19% |
| R22 | 3 | 34 | 200 | 17% |
| R23 | 4 | 35 | 200 | 17% |
| R24 | 2 | 33 | 200 | 16% |
| R25 | 5 | 35 | 200 | 18% |
| R26 | 3 | 33 | 200 | 17% |

Notes: [1] The 90th percentile background concentration is from the years 2001-2005 from NAPS Station No. 46089 (Brampton).

[2] The MOE's 24-Hour AAQC for NO_x is 200 µg/m³.