



Consulting Geotechnical & Environmental Engineering Construction Materials Inspection & Testing

GEOTECHNICAL REPORT DERRY ROAD AND ARGENTIA ROAD INTERSECTION IMPROVEMENTS REGION OF PEEL, ONTARIO

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Attention: Mr. Andrew O'Connor

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1.0 INTRODUCTION

Terraprobe Inc. (Terraprobe) has been retained by HDR Corporation (HDR) to provide geotechnical engineering services in support of the proposed intersection improvements at Derry Road and Argentia Road in the Region of Peel, Ontario. A site location plan is provided as Figure 1 and site photographs are presented in Figures 2 and 3.

The scope of work for the geotechnical engineering services is outlined in Terraprobe's proposal titled "Schedule 'B' Municipal Class EA for Derry Road and Argentia Road From 300m of All Quadrants of the Intersection, RFP 2013-261P, City of Mississauga, The Regional Municipality of Peel' dated May 10, 2013.

The purpose of this investigation was to explore the subsurface conditions within the study area by borehole drilling and pavement coring, in-situ testing and laboratory testing on soil samples. The data obtained from this investigation was used to provide Borehole Location Plan, Borehole Logs, laboratory test results, a description of the subsurface conditions and geotechnical design recommendations.

A geotechnical investigation was carried out for a section of Derry Road within the current project limits and selected data from this investigation is provided in this report. The following document is referenced in the preparation of this report:

 SPL Consultants Limited, "Geotechnical Investigation, Derry Road between Argentia & Millcreek, City of Mississauga, Ontario" Project No. 592-1078, dated February 25, 2013.

2.0 PROJECT AND SITE DESCRIPTION

Derry Road is an east/west oriented arterial road that intersects Argentia Road. This intersection is located in a full developed area with hotels at the northeast and southeast quadrants and commercial enterprises at the remaining quadrants of the intersection. A Highway 401 overpass and a railway bridge are located at the east and west limits of the study area respectively. Both roadways currently conform to an urban cross-section.

The purpose of this study is to identify long term improvements on the intersection for the horizon year of 2031 and, geotechnical consulting services are required to support the design.

3.0 SITE INVESTIGATION AND FIELD TESTING

The site investigation and field testing were carried out on June 6 and 9, 2014, and consisted of drilling and sampling twenty eight boreholes to depths ranging from approximately 0.6 m to 1.8 m below ground surface including asphalt pavement coring at four locations. The approximate borehole and corehole locations are shown on Figure 4 with the approximate locations of SPL's Boreholes from the referenced report.

The borehole and corehole locations were marked in the field by Terraprobe's field staff in relation to existing features shown on the base plan provided by HDR. Utility clearances and permits were obtained by Terraprobe prior to drilling.

On the existing roadways the boreholes were drilled with a CME 75 truck-mounted drill rig supplied and operated by Strong Soil Search of Claremont, Ontario. These borings were extended through the asphalt pavement and the overburden soils using solid stem augering techniques and soil



samples were obtained at selected intervals of depth using a 50 mm outer diameter (O.D.) splitspoon sampler in conjunction with the Standard Penetration Test (SPT) procedures as specified in ASTM Method D1586¹. Cores of the existing pavement were obtained with a 150 mm diameter core barrel.

The boreholes in the boulevard areas were extended manually by advancing a split-spoon sampler with portable hand operated vibratory equipment (Pionjar) supplied and operated by Sonic Soil Sampling of Concord, Ontario. Ground water conditions in the open boreholes were observed during and immediately following the drilling operations.

A member of Terraprobe's technical staff observed and recorded the borehole drilling and the sampling operations on a full-time basis. The soil samples were visually inspected in the field, placed in labelled plastic containers and transferred to Terraprobe's Brampton laboratory for further examination and testing.

The recovered soil samples were subjected to Visual Identification (VI) and select soil samples were subjected to a laboratory testing programme consisting of natural water content and grain size distribution in accordance with MTO and/or ASTM Standards as appropriate. The results of the soil testing program are presented on the Borehole Logs in Appendix A and on the figures in Appendix B. Two soil samples were also submitted to Agat Laboratories for soil chemical testing to assess soil disposal options for excess soils generated during construction. The results of the soil chemical tests are provided in Appendix D.

A visual pavement condition survey of Derry Road and Argentia Road was completed in August 2014. The survey was conducted in accordance with the procedures outlined in the Ministry of Transportation of Ontario (MTO) *Manual for Condition Rating of Flexible Pavements - Distress Manifestations (SP-024).* The Flexible Pavement Condition Evaluation Forms are included in Appendix C.

4.0 SUBSURFACE CONDITIONS

4.1 General

Reference is made to the Borehole Logs and Core Logs in Appendix A. Details of the encountered pavement structure and soil stratigraphy are provided in this appendix. An overall description of the pavement structure and soil stratigraphy is given in the following paragraphs. However; the factual data presented in the Borehole Logs and Core Logs governs any interpretation of the site conditions. The subsurface conditions will vary between and beyond the borehole locations.

¹ ASTM D1586 – Standard Test Method for Standard Penetration Tests and Split Barrel Sampling of Soils.



4.1.1 Pavement Structure

Pavement Component	Derry Road East Leg	Derry Road West Leg	Argentia Road North Leg	Argentia Road South Leg
HMA (mm)	165	120*	145	170
Granular (mm)	630	*	525	585
Total (mm)	795	*	670	755

The average pavement structures of the roadways are summarized below.

* The average asphalt thickness was derived from SPL Core Logs. Information on pavement granular thickness was not provided.

The granular material comprising the base/subbase courses of the roadways generally consists of gravelly sand to sand and gravel fill material. The pavement boreholes extended through the south leg of Argentia Road (Boreholes 16, 17, 22 and 23) encountered beneath the asphaltic concrete a sand layer that ranges from 560 mm to 620 mm in thickness. The locations, fill thickness and the range of SPT N-values and moisture contents are summarized below.

Borehole No.	Fill Thickness (m)	Range of SPT N- values (blows/0.3m)	Range of Moisture Content (% by weight)
8	0.64	41	-
9	1.04	21 – 48	-
12	0.89	23 – 46	-
13	0.62	49	-
16	0.62	28	4
17	0.60	31	-
22	0.56	23	-
23	0.57	14	-
26	0.43	17	-
27	0.41	17	-
31	0.60	21	-
34	0.65	19	5

Gravelly Sand to Sand and Gravel Fill

Two (2) samples of this gravelly sand to sand and gravel fill were subjected to grain size distribution tests and the results are presented in Figure B1 in Appendix B. The results are compared to the Ontario Provincial Standards (OPSS) Granular A and Granular B Type I specifications. Based on the SPT N-values the relative density of the gravelly sand, to sand and gravel fill is described as generally compact with occasional dense zones.



4.1.2 Topsoil

Topsoil thicknesses were measured in the widening areas beyond the existing pavement platform and the topsoil thickness ranged from 150 mm to 280 mm. Topsoil thickness may vary between and beyond the borehole locations.

4.1.3 Concrete

Boreholes 10 and 11 were drilled through the concrete sidewalk because of space restrictions and underground utilities in the general area. The concrete sidewalk is about 140 mm to 150 mm thick and is underlain by granular material that ranges from 410 mm to 1080 mm in thickness.

4.1.4 Fill – Sand and Gravel to Silty Sand

Sand and gravel to silty sand fill material were encountered below the topsoil and concrete sidewalk. The locations, fill thickness and moisture contents are summarized below.

Borehole No.	Fill Thickness (m)	Range of Moisture Content (% by weight)
4	0.6	-
7	0.4	14
10	0.4	6
11	1.1	-
20	0.7	-

Sand and Gravel to Silty Sand Fill

4.1.5 Fill – Silty Clay

Silty clay fill material was encountered within the project limits and the locations, fill thickness, range of SPT N-values and moisture contents are summarized below.

Silty Clay Fill

Borehole No.	Fill Thickness (m)	Range of SPT N- values (blows/0.3m)	Range of Moisture Content (% by weight)			
17	1.0*	4 – 11	13			
18	0.4*	-	-			
19	0.4	-				
20	0.6*	-	-			
21	0.3	-	-			
24	0.9	-	-			
25	0.4	-	-			
28	0.7	-	-			
29	0.4	-	-			
30	0.4	-	11			
32	0.3	-	-			



Borehole No.	Fill Thickness (m)	Range of SPT N- values (blows/0.3m)	Range of Moisture Content (% by weight)
33	0.4	-	-
34	0.4	10	-

*Borehole termination depth.

Based on the SPT N-values, the consistency of the silty clay fill is described as firm to stiff.

4.1.6 Till - Silty Clay

A silty clay till deposit was encountered across the site. Summarized below are the locations where these soils were found, their explored depths, range of SPT N-values and moisture contents.

Borehole No.	Depth of Deposit (m)	Range of SPT N- values (blows/0.3m)	Range of Moisture Content (% by weight)
4	1.8*	-	-
7	1.8*	-	14
8	1.6*	23 – 72/22.5 cm	-
9	1.8*	33	-
10	1.8*	-	15
11	1.7*	-	-
12	1.8*	32	-
13	1.8*	13 – 26	-
15	0.9*	-	-
16	1.7*	12 – 74/27.5 cm	11 - 16
19	1.5*	-	-
21	1.8*	-	-
22	1.6*	10 – 99/22.5 cm	-
23	1.8*	11 – 15	-
24	1.8*	-	-
25	1.1*	-	-
26	1.8*	65 – 77	-
27	1.8*	55 – 59	-
28	1.5*	-	-
29	1.1*	-	-
30	1.7*	-	14
31	1.8*	22 – 45	-
32	1.1*	-	-
33	1.1*	-	-
34	1.8*	22	-

Silty Clay Till

*Borehole termination depth.



Two samples of the silty clay till were subjected to grain size distribution tests and the results are presented in Figure B2 in Appendix B. These results show a soil matrix consisting of 0 - 2 % gravel, 17 - 22 % sand, 51 - 53 % silt and 25 - 30 % clay sized particles. Till soils can also be expected to contain random cobble and boulder inclusions.

Based on the SPT N-values the consistency of the silty clay till is described as stiff to hard.

4.2 Ground Water Levels

No free water was encountered in any of the boreholes during drilling. The ground water level is expected to fluctuate seasonally and will be influenced by major weather events and perched water can be expected to occur where surficial layers of gravelly sands are underlain by relatively impermeable silty clay soils.



5.0 DISCUSSION AND RECOMMENDATIONS

5.1 General

This section of the report presents an interpretation of the factual geotechnical data and provides geotechnical design recommendations. These discussions and recommendations are based on our understanding of the project, and our interpretation of the factual data obtained from the current and previous subsurface investigations.

Where comments are made on construction, they are provided to highlight those aspects that could affect the design of the project, and for which special provisions or operational constraints may be required in the Contract Documents. Those requiring information on the aspects of construction should make their own interpretation and assessment of the geotechnical information provided, as such interpretation may affect equipment selection, proposed construction methods, scheduling and the like.

HDR's design drawings illustrate that the intersection is to be upgraded by providing additional turning lanes on each leg of the intersection. The east and west legs of Derry Road will be widened on the south sides to accommodate additional left turn lanes. The south leg of Argentia Road will be widened on the east side to accommodate a new northbound through lane. The north leg of Argentia Road will be widened on the west side to accommodate a right turn lane.

5.2 Pavement Condition

A visual pavement condition evaluation of Derry Road and Argentia Road was completed in August 2014. The survey was conducted in accordance with the procedures outlined in the Ministry of Transportation of Ontario (MTO) *Manual for Condition Rating of Flexible Pavements - Distress Manifestations (SP-024).* The Pavement Condition Evaluation Forms are included in Appendix C. Summarized below are the observed pavement distresses and the overall pavement condition of the evaluated pavement sections.

Section	Overall Condition	General Distresses
Derry Road Sta. 9+720 to Sta. 10+166	PCR = 70, RCR = 7 Good	 Intermittent slight raveling and coarse aggregate loss. Intermittent slight wheel track rutting. Intermittent slight single and multiple longitudinal wheel track cracking. Intermittent slight transverse cracking.
Argentia Road Sta. 1+790 to Sta. 2+280	PCR = 70, RCR = 7 Good	 Frequent moderate raveling and coarse aggregate loss. Intermittent slight wheel track rutting. Intermittent slight single and multiple longitudinal wheel track cracking. Intermittent moderate alligator pavement edge cracking. Intermittent slight transverse cracking.

Summarized Pavement (Conditions
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5.3 Traffic Data

The AADT values, annual growth rates and percentage of commercial vehicles used for the pavement design were provided by HDR. This traffic data and the derived Equivalent Single Axle Loads (ESALs) are provided in the following table.



Parameters	Derry Road	Argentia Road
Projected AADT (2015)	40,730	15,520
Projected AADT (2021)	43,240	16,480
Projected AADT (2031)	47,730	18,180
Annual Growth Rate (2015 – 2031)	1%	1%
Percent Commercial Vehicles	5%	5%
Design ESALs (2021)	2,100,000	516,300
Design ESALs (2031)	5,050,000	1,450,000

Traffic Data and ESAL's

5.4 Pavement Designs

The pavement structures were designed based on the traffic information provided by HDR and the data obtained from the field investigations. Pavement designs were carried out for new construction (widening) as well as rehabilitation of the existing roadway.

The following references and guidelines were used for the pavement designs.

- MTO's "Adaptation and Verification of AASHTO Pavement Design Guide for Ontario Conditions, MI-183", March 19, 2008; and
- American Association of State Highway and Transportation Officials, "AASHTO Guide for Design of Pavement Structures", 1993.

The pavement design parameters are summarized in the following table.

Design Parameter	Values							
Initial/Terminal Serviceability Index	$P_i = 4.2$ $P_t = 2.2$							
Loss in Serviceability Index	2.0							
Desired Reliability (R %) and Standard Deviation (SD)	R = 85 SD = 0.45							
Estimated Resilient Modulus of Subgrade Soil (MPa)	35							
Layer Coefficients of Hot Mix Asphalt (HMA)	New HMA = 0.42 Existing HMA = 0.25 to 0.30							
Layer Coefficient of Granular Materials	Gran. A = 0.14 Gran. B Type I = 0.09 Existing Granular 'A' Material = 0.10 to 0.14 Existing Granular 'B' Material = 0.08							
Drainage Coefficient of Granular Materials	New Granular = 1.0 Existing Granular = 0.9 to 1.0							

AASHTO Pavement Design Parameters



5.4.1 Pavement Structures (New Construction – Widening)

Based on our pavement condition survey both roads are in good condition and have performed well over the years which likely indicates a structurally adequate pavement structure. Furthermore, since the turning traffic volume is less than the traffic volume in the main lanes; a pavement structure similar to the main lanes of the roadways will suffice. Existing and new pavement structures of at least equal thicknesses are also required to provide positive lateral drainage across the pavement platform.

The recommended pavement structure for new construction (widening) is:

Hot mix asphalt	HL-1 Surface Course DFC Surface Course HL-8 Binder Course	50 mm (except Argentia Road south leg) 50 mm (Argentia Road south Leg only) 100 mm
Granular A Base Cours Granular B Type I Sub Total thickness	base	150 mm 500 mm 800 mm
Granular Base Equival	ency	783 mm

5.4.2 Existing Pavement Rehabilitation

The structural capacities of the existing east leg of Derry Road and the north and south legs of Argentia Road were analyzed for the design traffic using AASHTO's pavement overlay design procedure. The structural capacities of the existing pavements are inadequate to support the design loads and pavement strengthening is required.

Consideration was given to strengthening the existing pavement by partial depth milling and repaving. The rehabilitation treatments for the existing pavements for service life extensions of 6 years and 16 years i.e. for horizon years 2021 and 2031 respectively are tabulated below:

Rehabilitation Treatment	Derry East		Derry West	·	Argent North		Argentia Rd South Leg		
Horizon Year	2021	2031	2021	2031	2021	2031	2021	2031	
Mill existing pavement (mm)	50	90	*	*	50	50	50	50	
Overlay with HMA (mm)	50	100	*	*	50	50	50	50	
Structural Number Provided (mm)	106	123	*	*	101	101	101	101	
Design Structural Number (mm)	106	120	*	*	86	100	86	100	

Existing Pavement Rehabilitation

* Derry Road west leg was recently repaved and the existing pavement structure of this section of the roadway was not available when this report was written.

Rehabilitation by milling the existing pavement a partial depth of 50 mm and repaving with a 50 mm thick HMA overlay is adequate to sustain the design traffic loads for a service life extension to Year 2021 on the east leg of Derry Road and service life extensions to Year 2021 and Year 2031 for the north and south legs of Argentia Road. If a service life extension to Year 2031 is required on the east leg of Derry Road, we recommend milling the existing pavement a partial depth of 90 mm and repaving with a 50 mm thick HL-1 surface course and a 50 mm thick HL-8 binder course. This recommended rehabilitation strategy will result in a grade raise of 10 mm.



The asphalt core sample extracted from the south leg of Argentia Road (Borehole 16) show a surface course comprising of Dense Friction Course (DFC) asphalt. We believe that DFC was used as a surface course because of the heavy traffic loads from busses arriving at and departing from the GO Station facility on Argentia Road south of Derry Road. Therefore, for new construction (widening) and rehabilitation of the south leg of Argentia Road, we recommend a 50 mm thick DFC surface course.

6.0 RECOMMENDATIONS AND COSTRUCTION FEATURES

6.1 Pavement Structure and Material Types

The following mix types are considered suitable for this project.

HL-1 or Superpave 12.5 FC1	Surface Course (except Argentia Road south leg);
DFC or Superpave 12.5 FC2	Surface Course (Argentia Road south Leg only); and
HL-8 or Superpave 19	Binder Course.

Granular A material should be used as base material for all new roadways and Granular B Type I is recommended as subbase material. Both the Granular A and the Granular B Type I materials should meet the OPSS.MUNI 1010 specifications.

SP 12.5 FC1, SP 12.5 FC2 and SP 19 hot mix asphalt types should be designed for Traffic Category C in accordance with OPSS MUNI 1151.

6.2 Padding

Superpave 9.5 (or alternatively HL 3HS for Marshall mixes) is recommended as padding. Padding should be placed in lifts not exceeding 50 mm below binder courses.

6.3 Asphalt Cement Grade

Performance graded asphalt cement PG 64-28 conforming to OPSS MUNI 1101 requirements, is recommended for the HMA binder and surface courses.

6.4 Routing and Sealing & Tack Coat

After milling, all cracks wider than 3 mm should be routed and sealed and a tack coat applied to the milled surface prior to placing the overlay.

A tack coat (SS1) should be applied to all construction joints prior to placing hot mix asphalt to create an adhesive bond. Prior to placing hot mix asphalt SS1 tack coat must also be applied to all existing or milled surfaces and between all new lifts.

6.5 Key-in Detail

Asphalt joint between the existing pavement and new construction should be constructed in accordance with applicable Region of Peel standards. Alternatively, a longitudinal key-in can be considered between the existing pavement and new construction.



6.6 Pavement Crossfall

The finished pavement surface should be adequately sloped (normally 2%) towards the sides to provide positive drainage. Continuity of drainage through the granular road base and subbase layers should be maintained between the existing and new pavement structures. In this regard, the granular thickness for any new pavement structure may have to be increased from the above recommended thickness in some areas to match any thicker granular fill encountered under the existing pavement.

6.7 Pavement Tapers

At the limits of construction, appropriate tapering of the pavement thickness to match the existing pavement structure should be implemented in accordance with OPSS or applicable Region and City's standard.

6.8 Subdrains

Since the widened roadways will conform to an urban section, full-length subdrains placed beneath the curb in accordance with OPSD 216.021 are required to provide pavement drainage. The subdrains should be connected to a positive outlet.

6.9 Compaction of Base & Sub-Base Materials

All granular base and subbase materials should be placed in 150 mm lifts and compacted to 100% of the material's Standard Proctor Maximum Dry Density (SPMDD) at $\pm 2\%$ of its Optimum Moisture Content (OMC). Asphalt concrete should be placed and compacted in accordance with the appropriate OPSS or Region of Peel and City of Mississauga specifications.

6.10 Reuse of Existing Granular Fill

It is envisaged that some of the existing granular material below the roadways would be salvaged during construction operations. The grain size analyses of two selected samples (Figure B1, Appendix B) of the existing pavement base and sub-base granular material indicate that the material does not meet the OPSS 1010 specifications for Granular 'A' and the fines content also exceeds the allowable fines content for OPSS 1010 Granular B Type I material. Therefore, this granular fill cannot be used as Granular 'A' or Granular 'B' for pavement construction. However, the granular material can be used as fill elsewhere on this project provided it is free of topsoil, organics and other deleterious material.

6.11 Excavations

All excavations must be carried out in accordance with the Occupational Health and Safety Act (OHSA). For the purposes of the OHSA, the soils at this site may be classified as:

- Fill material Type 3 soil.
- Silty Clay Till Type 2 soil.



6.12 Stripping

For estimating purposes assume an average topsoil thickness of 200 mm in the widening areas.

6.13 Subgrade Preparation

All topsoil, organics, soft/loose and otherwise disturbed soils should be stripped from the subgrade areas. The exposed subgrade is expected to consist of silty clay fill, sand and gravel to silty sand fill and native silty clay till. The silty clay fill and native silty clay till soils are fine-grained soils and will be weakened by construction traffic when wet; especially if site work is carried out during periods of wet weather. During these weather conditions, an adequate granular working surface would be required in order to minimize subgrade disturbance. Subgrade preparation and fill construction should not be done in the winter.

Immediately prior to placing the granular base, the exposed subgrade should be compacted and then proof-rolled with a heavy rubber tired vehicle (such as a loaded gravel truck). The subgrade should be inspected for signs of rutting or displacement. Areas displaying signs of rutting or displacement should be re-compacted and retested or, the material should be excavated and replaced with well-compacted and clean fill.

The fill may consist of either granular material or local inorganic soils provided that its moisture content is within $\pm 2\%$ of optimum. Fill should be placed and compacted in accordance with OPSS 501 and the final 300 mm of the subgrade should be compacted to 98% of SPMDD. The final subgrade surface should be sloped at least 3% to provide positive drainage.

6.14 Frost Protection

The grain size distribution results of the silty clay till indicate that the percentage of soil particles between 5 μ m and 75 μ m ranges from about 36% to 40%. Based on MTO's *Pavement Design and Rehabilitation Manual, SDO 90-01*, these soils are categorized as low to moderate frost susceptibility (LSFH to MSFH).

Based on *the City of Mississauga Standard No. 2220.020 Standard Frost Suitability of Soils,* these soils are assigned a frost value of 11.

For design purposes assume a frost penetration depth of 1.2 m.

6.15 Backfill

The native soils, the earth fill and the existing granular fill will generally be suitable for use as backfill materials provided they are free of topsoil, organics or other deleterious material.

To achieve the specified compaction, soils must neither be too wet nor too dry of their optimum moisture content. Soils that are too wet cannot be used immediately because the material will have to be dried to about ± 2 % of the optimum moisture content. If the construction operations are time sensitive, the use of imported granular material may be considered. Soils that are dry of optimum can be used immediately provided that the material is moisture conditioned (i.e. water added) to achieve a moisture content of ± 2 % of optimum.

Topsoil encountered at the site may be stockpiled and reused for landscaping purposes.



7.0 SOIL CHEMICAL ANALYSIS

Two soil samples were submitted to Agat Laboratories for chemical characterization with respect to general inorganic parameters including metals, pH, sodium adsorption ratio (SAR) and electrical conductivity (EC) to assess options for reuse or disposal of excess soils that will be generated during construction. Based on visual and/or olfactory screening of soil samples, these nominal parameters are analysed when there are no indications of environmental impacts. However, additional sampling/testing will likely be required during construction to confirm disposal or re-use options. The Certificates of Analysis are included in Appendix D.

The analytical results were compared to Table 1 (Agricultural) of the MOE Soil, Ground Water and Sediment Standards for Use under Part XV.1 of the Environmental Protection Act, April 15, 2011. Comparison of the test results to the MOE Standard indicates that the SAR and electrical conductivity of Sample SS2B from Borehole 17 retrieved at a depth of 0.8 m - 1.2 m, exceeded the guideline values. The metal concentrations of both tested samples are below the remediation concentrations stipulated in Table 1. Refer to the Guideline Violation table in Appendix D for further details.

The conclusions herein are based on limited analytical data and the actual quality of the excavated soils could vary during construction. Debris or stained/odorous soils, that are encountered during excavation, should be segregated and re-evaluated for disposal or re-use as fill and may require additional chemical analysis.

The testing carried out was intended to provide an overview of the soil quality and may not be adequate for the design of a soil management plan for construction. The actual acceptance criteria for surplus soil will vary with the receiving site and additional analyses may be needed to satisfy site specific acceptance criteria.

8.0 LIMITATIONS AND RISK

8.1 Procedures

This investigation has been carried out using investigation techniques and engineering analysis methods consistent with those ordinarily exercised by Terraprobe and other engineering practitioners, working under similar conditions and subject to the time, financial and physical constraints applicable to this project. The discussions and recommendations that have been presented are based on the factual data obtained.

It must be recognized that there are special risks whenever engineering or related disciplines are applied to identify subsurface conditions. Even a comprehensive sampling and testing programme implemented in accordance with the most stringent level of care may fail to detect certain conditions. Terraprobe has assumed for the purposes of providing design parameters and advice, that the conditions that exist between sampling points are similar to those found at the sample locations. The conditions that Terraprobe has interpreted to exist between sampling points can differ from those that actually exist.

It may not be possible to drill a sufficient number of boreholes or sample and report them in a way that would provide all the subsurface information that could affect construction costs, techniques, equipment and scheduling.



8.2 Changes in Site and Scope

It must also be recognized that the passage of time, natural occurrences, and direct or indirect human intervention at or near the site have the potential to alter subsurface conditions. Ground water levels are particularly susceptible to seasonal fluctuations.

The discussion and recommendations are based on the factual data obtained from investigations made by Terraprobe and are intended for use by the owner and its retained designers in the design phase of the project. If there are changes to the project scope and development features the interpretations made of the subsurface information, the geotechnical design parameters and comments relating to constructability issues and quality control may not be relevant or complete for the revised project. Terraprobe should be retained to review the implications of such changes with respect to the contents of this report.

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9.0 CLOSURE

This report was prepared by Mr. H Ahmed, P.Eng., a Geotechnical Engineer with Terraprobe, and reviewed by Mr. Rehman Abdul, M.S., P.Eng., a Senior Geotechnical Engineer and Associate with Terraprobe.

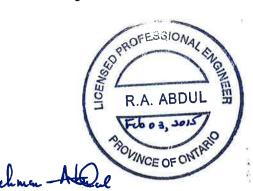
Terraprobe Inc.

H. Ahmed, P.Eng. Geotechnical Engineer









R. Abdul, P.Eng. Associate, Senior Geotechnical Engineer

REFERENCES

American Association of State Highway Officials, AASHTO Guide for Design of Pavement Structures, 1993.

ASTM D698-12, Standard Test Methods for Laboratory Compaction Characteristics of Soil Using Standard Effort, 2012.

ASTM D1586 - 08a, Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils, 2008.

Ontario Regulation 213/91, Occupational Health and Safety Act (OHSA) and Regulations for Construction Projects, April 11, 2012.

Ministry of the Environment, April 15, 2011. Soil, Ground Water and Sediment Standards for Use under Part XV.1 of the Environmental Protection Act, PIBS # 7382e01.

Ministry of Transportation Ontario, Adaption and Verification of AASHTO Pavement Design Guide for Ontario Conditions (MI-183), 2008.

Ministry of Transportation Ontario. Pavement Design and Rehabilitation Manual (SDO 90-01), 1990.

Ministry of Transportation Ontario, Manual for Condition Rating of Flexible Pavements - Distress Manifestations (SP-024), August 1989.

Ontario Provincial Standard Specifications (OPSS)

OPSS 501	Construction Specification for Compacting.
OPSS 1010	Material Specification for Aggregates – Base, Subbase, Select Subgrade and Backfill Material.
OPSS.MUNI 1010	Material Specification for Aggregates Base, Subbase, Select Subgrade and Backfill Material.
OPSS.MUNI 1101	Material Specification for Performance Graded Asphalt Cement.
OPSS.MUNI 1151	Material Specification for Superpave and Stone Mastic Asphalt Mixtures.

Ontario Provincial Standard Drawings (OPSD)

OPSD 216.021 Subdrain Pipe and Outlet Details.

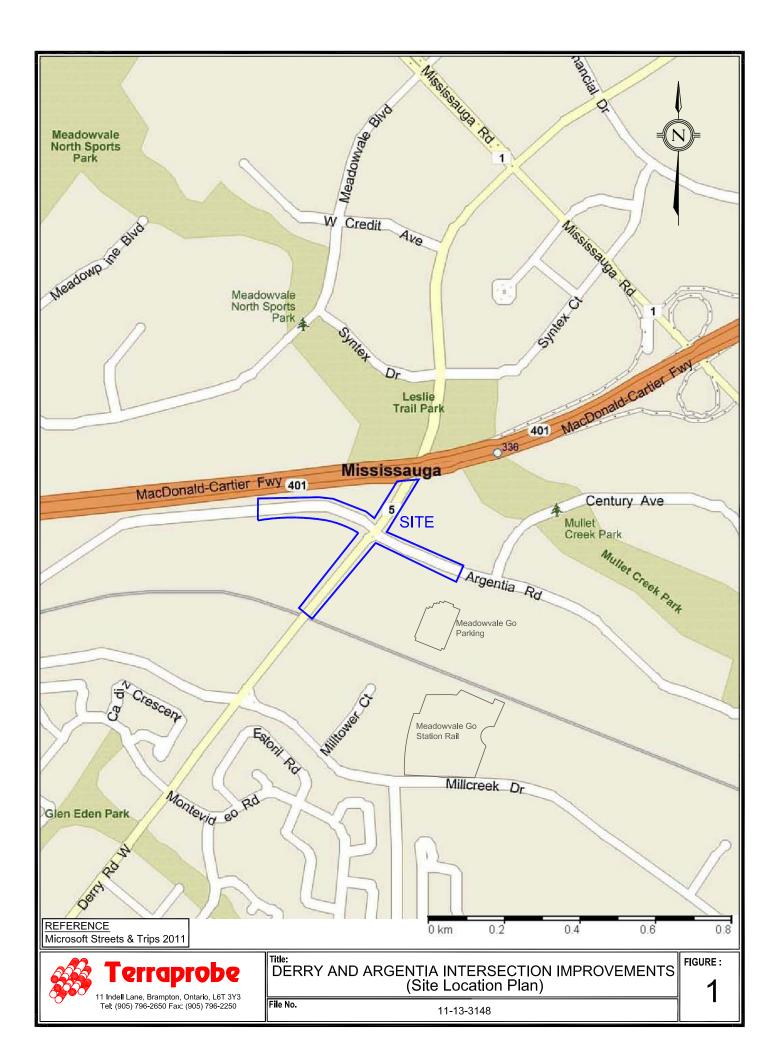
City of Mississauga T & W Standard Drawings

STANDARD No. 2220.010	Standard Pavement and Road Base Design Requirements.
STANDARD No. 2220.020	Standard Frost Suitability of Soils.



FIGURES





Derry and Argentia Roads Intersection Improvements



Photograph #1: Derry Road, Sta. 9+800 Approx., looking west



Photograph #2: Derry Road, Sta. 10+050 Approx., looking east



Derry and Argentia Roads Intersection Improvements

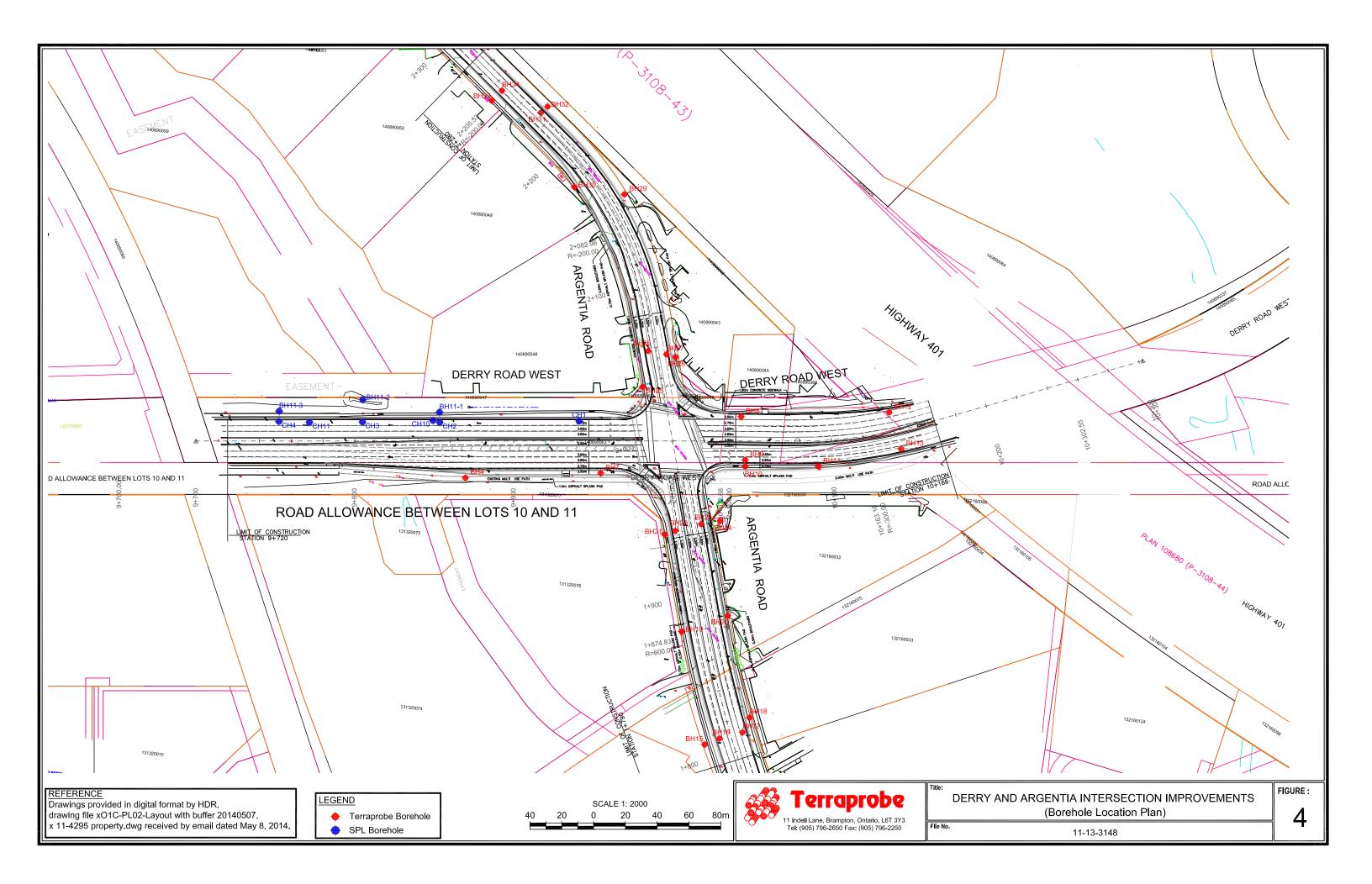


Photograph #3: Argentia Road, at South Limit, looking north



Photograph #4: Argentia Road, at North Limit, looking south





APPENDIX A



Terraprobe Borehole and Core Logs



SAMF	PLING METHODS	PENETRATION RESISTANCE
AS GS SS ST WS	Auger sample Grab sample Split spoon Shelby tube Wash sample	Standard Penetration Test (SPT) N-value (penetration resistance) is defined as the number of blows required to advance a standard 50 mm (2 in.) diameter split spoon sampler for a distance of 0.3 m (12 in.) with a hammer weighing 63.5 kg (140 lb.) falling freely for a distance of 0.76 m (30 in.).
RC SC	Rock core Soil core	Dynamic Cone Penetration Test (DCPT) resistance is defined as the number of blows required to advance a conical steel point 50 mm (2 in.) base diameter tapered 60° to the apex and attached to 'A' size drill rods for a distance of 0.3 m (12 in.), with a hammer weighing 63.5 kg (140 lb.) falling freely for a distance of 0.76 m (30 in.).

COHESIONLES	S SOILS	COHESIVE S	OILS	MINOR SOIL CONSTITUENTS					
Relative Density	N-value Blows/0.3m	Consistency	N-value Blows/0.3m	Undrained Shear Strength (kPa)	Modifier (e.g)	% by weight			
Very loose Loose Compact Dense Very dense	< 5 5 – 10 10 – 30 30 – 50 > 50	Very soft Soft Firm Stiff Very stiff Hard	< 2 2 - 4 4 - 8 8 - 15 15 - 30 > 30	< 12 12 – 25 25 – 50 50 – 100 100 – 200 > 200	<i>trace</i> (trace silt) <i>some</i> (some silt) (ey) or (y) (sandy) <i>and</i> (sand and silt)	< 10 10 – 20 20 – 35 > 35			

TESTS AND SYMBOLS

МН	combined sieve and hydrometer	Ā	Unstabilized water level
	analysis	Ţ	1 st water level measurement
W,	water content	<u> </u>	
w _L ,	liquid limit	$\bar{\mathbf{\Lambda}}$	2 nd water level measurement
W _P ,	plastic limit	▼	Most recent water level measurement
I _P ,	plasticity index	-	
k	coefficient of permeability	^{3.0} +	Undrained shear strength from field vane (with sensitivity)
γ	soil unit weight, bulk	Cc	compression index (normally consolidated range)
Gs	specific gravity	Cr	recompression index (overconsolidated range)
Φ'	effective angle of internal friction	Cv	coefficient of consolidation
c'	effective cohesion	mv	coefficient of compressibility (volume change)
Cu	undrained shear strength (Φ = 0 analysis)	е	void ratio

FIELD MOISTURE DESCRIPTIONS

Dry	refers to a soil sample with a moisture content well below optimum ($w < w_{opt}$), absence of moisture, dusty, dry to the touch.
Moist	refers to a soil sample with a moisture content at or near optimum (w \approx w _{opt}), no visible pore water.
Wet	refers to a soil sample with a moisture content well above optimum (w > w _{opt}), has visible pore water.



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 4

Project No.: 11-13-3148

Date started : June 9, 2014

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	n : E: 600277, N: 4828231 (UTM 17	T)				Elevatio	on Datu	m : I	N/A											
Rig typ	e : PIONJAR SOIL PROFILE	к	ш	DYNAMIC CONE PENETRATION RESISTANCE PLOT								ΝΑΤΙ	IRAI							
ELEV DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEA ○	20 R STR UNCO QUICK	4 <u>0</u> ENGTH NFINED	60 (kPa)	8 <u>0</u> +) 1(FIELD	Q0 D VANE VANE Q0	WA			LIQUID LIMIT W _L T (%)	τη Nult Meight kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	250mm TOPSOIL	<u>17</u>	•																	
0.3	FILL, silty sand, trace gravel, brown, damp		1	SS																
	sand and gravel below		2A	SS																
0.9	SILTY CLAY, sandy, trace gravel, brown, moist (GLACIAL TILL)		2B		-															
1.8	containing shale fragments, reddish brown below		3	SS																

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 7

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600328, N: 4828300 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w ELEV DEPTH (m) 20 Wp w ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) γ ○ UNCONFINED● QUICK TRIAXIAL + FIELD VANE \times LAB VANE WATER CONTENT (%) kN/m³ 20 40 60 80 100 10 20 30 GROUND SURFACE GR SA SI CL 14 150mm TOPSOIL 0.2 FILL, gravelly sand, some silt, brown, damp 0 1 SS ...silty clay, moist below 0.6 SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL) 2 SS SS 3 0

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 8

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positio	Position : E: 600355, N: 4828391 (UTM 17T) Elevation Datum : N/A																	
Rig typ	Rig type : CME 75, truck-mounted Drilling Method : Solid stem augers																	
	SOIL PROFILE		S	SAMPL	ES	К Ши	щ	DYNAMIC CONE PENETRATION RESISTANCE PLOT						NATU	RAL			
ELEV DEPTH (m)		STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	20 SHEAR STRI O UNCO ● QUICK	4 <u>0</u> ENGTH NFINED	<u>60</u> (kPa) AL	80 1 + FIELI × LAB		WA	IC NATU MOIST CONT W TER CO		LIQUID IMIT WL T (%)	ν γ κN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 200mm ASPHALTIC CONCRETE														<u> </u>			GR SA SI CL
0.2	640mm FILL-SAND AND GRAVEL, some silt, dense, brown, damp		1	SS	41													
0.8	SILTY CLAY, some sand, trace gravel, very stiff to hard, brown, moist (GLACIAL TILL)		2	SS	23													
1.6			3	SS	72 / 225mm													at 1.6m, sampler bouncing /

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 9

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positio	Position : E: 600378, N: 4828376 (UTM 17T) Elevation Datum : N/A Rig type : CME 75, truck-mounted Drilling Method : Solid stem augers																		
Rig typ	e : CME 75, truck-mounted	Drilling	Methoo	1:5	Solid s	tem a	ugers												
SOIL PROFILE SAMPLES						Ľ.	щ	DYNA RESIS	MIC CC	NE PER	NETRA	FION		DIACT		URAL	LIQUID		
<u>ELEV</u> DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAI O	0 R STRE UNCO QUICK	10 (Ength NFINED TRIAXI/	<u>50</u> (kPa)	30 1 + FIELI × LAB	00 D VANE		TER CO	w o ONTEN	LIMIT W _L	N/m ³ WEIGHT	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	180mm ASPHALTIC CONCRETE																		
0.2	1040mm FILL-GRAVELLY SAND , some silt, compact to dense, brown, damp		1	SS	48														
			2	SS	21														
1.2	SILTY CLAY, some sand, trace gravel, hard, brown, moist (GLACIAL TILL)		3	SS	33														

END OF BOREHOLE



: HDR Corporation Client

Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

Project No.: 11-13-3148 Date started : June 9, 2014 Sheet No. : 1 of 1

LOG OF BOREHOLE 10

Position : E: 600381, N: 4828373 (UTM 17T) Elevation Datum : N/A Rig type : PIONJAR																			
	SOIL PROFILE	н.	щ	DYNAM	MIC CON	NE PEI PLOT	NETRA	TION			- NATI	JRAI							
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2(SHEAF	0 4 <u>0</u> R STREI UNCONI QUICK 1) (NGTH FINED FRIAXI	<u>50</u> (kPa) AL	8 <u>0</u> + FIEL × LAB				TENT W O ONTEN		λ Weight	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 150mm CONCRETE SIDEWALK	₽. ь					ш	20	0 40) (50	80 ⁻	100	1	0 2	20	30	kN/m ³	GR SA SI CL
0.2	410mm FILL-SAND AND GRAVEL, some silt, brown, damp SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL)		2	SS										0	0				2 17 51 30
			3	SS															

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 11

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

Positio Rig typ	,	.)				Elevatio	on Datu	ım : I	N/A										
	SOIL PROFILE	_	5	SAMPL	ES	ц Ш.	щ	DYNA RESIS	MIC CO	NE PE	NETRA	ATION		DI AGT	o NATU	JRAL			
ELEV DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	SHEA	20 4 R STRE UNCOM QUICK	<u>IO</u> INGTH IFINED TRIAXI	6 <u>0</u> (kPa)	80 1 + FIEL × LAB				v DNTEN	LIQUID LIMIT W _L T (%)	Δ MEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	140mm CONCRETE SIDEWALK																		
	1080mm FILL-GRAVELLY SAND, some silt, containing clay lumps, brown, moist		1	SS	-														
			2	SS															
1.2	SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL)		3	SS															
1.7	END OF BOREHOLE	<u>v · D ·</u>											·						



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 12

Project No.: 11-13-3148

Sheet No. :

Date started : June 6, 2014

1 of 1

Positic	on : E: 600411, N: 4828466 (UTM 171	Γ)				Elevatio	on Datu	m : 1	N/A								
Rig typ	e : CME 75, truck-mounted					Drilling	Method	1 : 8	Solid s	tem a	ugers	;					
	SOIL PROFILE SAMPLES						щ	DYNA RESIS	MIC CO	NE PE PLOT	NETRA	ATION	PLASTIC NAT	URAL	LIQUID		
ELEV DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEA O	<u>0</u> 4 R STRE UNCON QUICK	0 NGTH IFINED TRIAXI	6 <u>0</u> (kPa) AL	80 1 + FIELI × LAB		ITENT W O ONTEN	LIMIT W _L	NNIT UNIT م WEIGHT	REMARKS & GRAN SIZE DISTRIBUTION (%) GR SA SI CL
	155mm ASPHALTIC CONCRETE																
0.2	890mm FILL-GRAVELLY SAND, some silt, compact to dense, brown, damp		1	SS	46												
1.0	SILTY CLAY, some sand, trace		2A 2B	SS	23												
	gravel, very stiff to hard, brown, moist (GLACIAL TILL)		20			-											
			3	SS	32												

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

LOG OF BOREHOLE 13

Project No.: 11-13-3148

Sheet No. :

Date started : June 6, 2014

1 of 1

Location : Mississauga, Ontario

osition	E: 600434, N: 4828457 (UTM 17T)				Elevatio	on Datu	m : N	N/A										
ig type	e : CME 75, truck-mounted					Drilling	Method			stem a	-								
	SOIL PROFILE		s	AMPL	ES	Щ.	щ	DYNA RESIS	MIC CO	DNE PE E PLOT	NETR	ATI	ON		PLASTI	JRAL	LIQUID		
LEV PTH m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	⊖ ●	R STRI UNCO QUICH	ENGTH NFINED		+	FIELD	VANE ANE	W _P WA	TENT N O ONTEN	LIMIT W _L	ν κN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI
	155mm ASPHALTIC CONCRETE																		
	620mm FILL-GRAVELLY SAND, some silt, dense, brown, damp		1	SS	49	-													
	SILTY CLAY, some sand, trace gravel, stiff to very stiff, brown, moist (GLACIAL TILL)		2A 2B	SS	13														
			3	SS	26														
1.8			3	SS	26														

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 15

Project No.: 11-13-3148

Date started : June 9, 2014

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	n : E: 600503, N: 4828244 (UTM 17 e : PIONJAR	T)				Elevatio	on Datu	m : N/A
ELEV DEPTH (m)	SOIL PROFILE DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	BAMPL Bak	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$
0.2	150mm TOPSOIL SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL)		1	SS SS				
0.9	END OF BOREHOLE Unable to drill borehole deeper		1			[]	
	Borehole was dry and open upon completion of drilling.							



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 16

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positio	n : E: 600505, N: 4828254 (UTM 171)			I	Elevatio	n Datu	m : N	N/A										
Rig typ	e : CME 75, truck-mounted				I	Drilling	Method	1:8	Solid st	tem a	ugers	3							
SOIL PROFILE SAMPLES							щ	DYNA RESIS	MIC CO	NE PEI PLOT	NETR	ATION			NAT	URAL			
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAI O	0 4 R STRE UNCON QUICK	0 (NGTH IFINED TRIAXI	6 <u>0</u> (kPa) AL	80 + File × LA	100 ELD VANE B VANE	WA	TER CO		. ,	λ weight	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 180mm ASPHALTIC CONCRETE								0 4	0 (60	80	100	1	0 2	20	30	kN/m ³	GR SA SI CL
	180mm ASPHALTIC CONCRETE																		
0.2	620mm FILL-SAND, some silt, trace clay, trace gravel, compact, grey, damp		1	SS	28									0					7 70 (23)
0.8	SILTY CLAY, some sand, trace gravel, stiff to hard, brown, moist (GLACIAL TILL)		2	SS	12										0				
1.7	reddish brown below		3	SS	74 / 275mm										0				

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

LOG OF BOREHOLE 17

Project No.: 11-13-3148

Sheet No. :

Date started : June 6, 2014

1 of 1

Location : Mississauga, Ontario

Positio	on : E: 600511, N: 4828268 (UTM 17	T)				Elevatio	on Datu	m : N	√A/										
Rig typ	e : CME 75, truck-mounted					Drilling	Methoo	1:5	Solid s	tem a	ugers	5							
	SOIL PROFILE	-	5	SAMPL	ES	E	щ	DYNA RESIS	MIC CO TANCE	NE PEI PLOT	NETR/	ATION	l	DLAST		JRAL	LIQUID		
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAI O	0 4 R STRE UNCON QUICK 0 4	<u>0</u> NGTH IFINED TRIAXI/	50 (kPa)	8 <u>0</u> + FI	- 100 IELD VANE AB VANE 100	WA	CON TER CO	TENT w o ONTEN	LIMIT WL	NUL MEIGHT KN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	180mm ASPHALTIC CONCRETE																		
0.2	600mm FILL-SAND , some silt, trace clay, trace gravel, dense, grey, damp		1	SS	31	-													
0.8	FILL, silty clay, some sand, trace gravel, containing shale fragments, firm to stiff, reddish brown, moist		2A 2B	SS	11														
			3	SS	4										0				

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 18

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No.: 1 of 1

Positio	on : E: 600507, N: 4828277 (UTM 17	T)				Elevatio	on Datu	im : N	J/A										
Rig ty	be : PIONJAR																		
	SOIL PROFILE		S	AMPL	ES	ĸ	ш	DYNA RESIS	VIC CO	NE PEN PLOT	IETRA	TION			ΝΔΤΙ	IRAI			
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAF O	0 4 R STREI UNCON QUICK	0 <u>6</u> NGTH (IFINED TRIAXIA	(0 kPa)	80 1 + FIEL × LAB	VANE				``	ν WIT WIT WIT WIT WIT WIT WIT WIT	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE	314						2	0 4	06		80 1	00	- 1	0 2	0	30	KIN/III	GR SA SI CL
0.2	200mm TOPSOIL FILL, silty clay, some sand, trace gravel, trace rootlets, brown, moist		1	SS															
0.6																			

END OF BOREHOLE

Borehole encountered obstruction at 0.6m and was moved within 2m radius around original location. Borehole was terminated at 0.6m after 3 attempts.



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 19

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

Positio	on : E: 600438, N: 4828277 (UTM 171)			I	Elevatio	on Datu	m : 1	N/A									
Rig typ	e : PIONJAR																	
	SOIL PROFILE		S	SAMPL	ES	R.	щ	DYNA RESIS	MIC CO	NE PEN PLOT	IETRA	TION		NAT	URAL			
ELEV DEPTH (m)		STRAT PLOT	NUMBER	түре	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEA ○	R STRE UNCON QUICK	<u>06</u> NGTH (IFINED TRIAXIA	j0 (kPa) AL	8 <u>0</u> 11 + FIELE × LAB \	W _P	TER CO	TENT w o DNTEN	LIQUID LIMIT W _L IT (%)	LH9 γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 150mm TOPSOIL	<u>717</u>																GR SA SI CL
0.2	FILL, silty clay, some sand, trace gravel, brown, moist		1	SS														
0.6	SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL)		2	SS														
	containing shale fragments, reddish brown below		3	SS														

END OF BOREHOLE

1.5



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 20

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600448, N: 4828306 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w ELEV DEPTH (m) 20 Wp w ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) γ + FIELD VANE \times LAB VANE ○ UNCONFINED● QUICK TRIAXIAL WATER CONTENT (%) kN/m³ 20 40 60 80 100 20 30 GROUND SURFACE 10 GR SA SI CL 11 130mm TOPSOIL FILL, silty sand, trace gravel, brown, damp SS 1 2A FILL, silty clay, some sand, trace gravel, brown, damp 0.8 SS 2B 3 SS no futher progress due to obstruction 1.4

END OF BOREHOLE

Unable to drill borehole deeper



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 21

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600383, N: 4828307 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w ELEV DEPTH (m) 20 Wp w ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) γ ○ UNCONFINED● QUICK TRIAXIAL + FIELD VANE \times LAB VANE WATER CONTENT (%) kN/m³ 20 40 60 80 100 20 30 GROUND SURFACE 10 GR SA SI CL 11 250mm TOPSOIL 1/ 1 0.3 SS FILL, silty clay, some sand, trace 1 gravel, brown, moist 0.6 SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL) 2 SS SS 3

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 22

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positio	n : E: 600386, N: 4828314 (UTM 17T)			I	Elevatio	on Datu	m : N	J/A									
Rig typ	e : CME 75, truck-mounted				I	Drilling	Methoo	1:8	Solid st	tem a	ugers							
	SOIL PROFILE		S	SAMPL	ES	и Ши	щ	DYNA RESIS	MIC CO TANCE	NE PE PLOT	NETRA	TION	PLASTIC	NATU	IRAL	LIQUID		
ELEV DEPTH (m)		STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAI O	0 4 R STRE UNCON QUICK	0 NGTH IFINED TRIAXI	6 <u>0</u> (kPa) AL	8 <u>0</u> 1 + FIELI × LAB	LIMIT W _P			LIMIT W _L	γ κN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 150mm ASPHALTIC CONCRETE								-	0				, 2	0 0		N. VIII	GR SA SI CL
0.2	560mm FILL-SAND , some silt, trace clay, trace gravel, compact, grey, damp		1	SS	23													
0.7	SILTY CLAY, some sand, trace gravel, stiff, brown, moist (GLACIAL TILL)		2	SS	10													
1.6	containing shale fragments, hard, reddish brown below		3	SS	99 / 225mm													

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 23

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positio	n : E: 600393, N: 4828329 (UTM 17	T)				Elevatic	n Datu	m : N	I/A										
Rig typ	e : CME 75, truck-mounted					Drilling	Methoo	1:5	Solid st	tem au	ugers								
	SOIL PROFILE		S	SAMPL	ES	и Ши	щ	DYNA RESIS	VIC CO TANCE	NE PEN PLOT	IETRA	TION		DI AOTI	o NATI	URAL			
<u>ELEV</u> DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEAF	0 4 R STRE UNCON QUICK	<u>0 6</u> NGTH (IFINED TRIAXI <i>I</i>	j0 (kPa) AL	80 1 ╋ FIEL × LAB	QO D VANE VANE QO	PLASTI LIMIT W _P WAT		TENT w o DNTENT	LIQUID LIMIT W _L T (%)	NNIT UNIT V سواط	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	180mm ASPHALTIC CONCRETE																		
0.2	570mm FILL-SAND , some silt, trace clay, trace gravel, compact, grey, damp		1	SS	14														
0.8	SILTY CLAY, some sand, trace gravel, stiff, brown, moist (GLACIAL TILL)		2A 2B	SS	11														
1.8	containing shale fragments, reddish \brown below		3	SS	15														

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 24

Project No.: 11-13-3148

Sheet No. :

Date started : June 9, 2014

1 of 1

Position : E: 600398. N: 4828340 (UTM 17T)

Positio Rig typ	, X	T)				Elevatio	on Datu	im : N	I/A										
	SOIL PROFILE		S	AMPL	ES	E S	Щ	DYNA RESIS	MIC CO TANCE		NETR/	TION		PLAST	IC NATU	JRAL	LIQUID		
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE		R STRE UNCON QUICK	NGTH	(kPa) AL	+ FIEL × LAB	100 _D VANE _ VANE 100	WA		TENT N D NTEN	LIMIT W _L	τη ν κN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI C
	230mm TOPSOIL	<u>x</u> 1 _Z																	GR SA SI C
0.2	FILL, silty clay, some sand, trace gravel, reddish brown, moist		1	SS															
	sand below		2A	SS															
1.1	SILTY CLAY, some sand, trace gravel, brown, moist		2B																
	(GLACIAL TILL)		3	SS															

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 25

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600302, N: 4828354 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w 20 Wp w ELEV DEPTH ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) (m) γ ○ UNCONFINED● QUICK TRIAXIAL + FIELD VANE \times LAB VANE WATER CONTENT (%) kN/m³ 20 40 60 80 100 20 30 GROUND SURFACE 10 GR SA SI CL 11 150mm TOPSOIL 0.2 FILL, silty clay, some sand, trace gravel, brown, moist SS 1 0.6 SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL) 2 SS 1.1 END OF BOREHOLE Unable to drill borehole deeper Borehole was dry and open upon completion of drilling.



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 26

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positic	on : E: 600286, N: 4828371 (UTM 17	T)				Elevatic	n Datu	m : 1	N/A										
Rig typ	e : CME 75, truck-mounted					Drilling	Method	1 : 5	Solid s	tem a	ugers								
	SOIL PROFILE		S	SAMPL	ES	Ľ.	щ	DYNA RESIS	MIC CC	NE PEI PLOT	NETRA	TION		DIACT	_ NAT	URAL	LIQUID		
ELEV DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	SHEA O	R STRE UNCOI QUICK	NGTH NFINED TRIAXI	(kPa) AL	+ FIE × LAI	100 ELD VANE B VANE 100		TER CO	W O ONTEN ⁻	LIMIT W _L	N/m ³ N/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CI
	140mm ASPHALTIC CONCRETE																		
0.2	430mm FILL-GRAVELLY SAND, some silt, compact, brown, damp SILTY CLAY, some sand, trace		1	SS	17														
	gravel, containing shale fragments, hard, reddish brown, moist (GLACIAL TILL)		2	SS	77														
1.8			3	SS	65														

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 27

Project No.: 11-13-3148

Sheet No. :

Date started : June 6, 2014

1 of 1

Positic	on : E: 600295, N: 4828379 (UTM 17	T)				Elevatio	on Datu	ım : I	N/A										
Rig typ	e : CME 75, truck-mounted					Drilling	Method	: t	Solid s	tem a	ugers								
	SOIL PROFILE		5	SAMPL	ES	н К К	щ	DYNA RESIS	MIC CO TANCE	NE PEI PLOT	NETRA	TION		DIACT		URAL			
ELEV DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	SHEA O	<u>0</u> 4 R STRE UNCOM QUICK	<u>0 (</u> NGTH IFINED TRIAXI	5 <u>0</u> (kPa) AL	8 <u>0</u> 1 + Fiel × LAB	100 .D VANE VANE 100		CON		LIQUID LIMIT W _L T (%) 30	LH9I3M γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI C
	140mm ASPHALTIC CONCRETE																		
0.2	410mm FILL-GRAVELLY SAND, some silt, compact, brown, damp		1A	SS	17														
0.5	SILTY CLAY, some sand, trace gravel, hard, brown, moist (GLACIAL TILL)		1B																
	containing shale fragments, reddish brown below		2	SS	55														
			3	SS	59														

END OF BOREHOLE

1.8



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 28

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

ELEV DEPTH (m) DESCRIPTION OI FUND SUBJECT M FUND SUBJEC M F	Positio	on : E: 600300, N: 4828382 (UTM 17T)				Elevatio	ion Dati	um : I	N/A											
$\frac{\text{ELEV}}{\text{DEPTH}} \text{DESCRIPTION} \left \begin{array}{c} U \\ u \\ v \\ m \end{array} \right \\ \frac{1}{230 \text{ mm}} \text{TOPSOIL} \\ 0.2 \\ \frac{1}{230 \text{ mm}} \text{TOPSOIL} \\ 0.2 \\ \frac{1}{224} \\ \frac{1}{24} \\ \frac{1}{2$	Rig typ	be : PIONJAR																			
$\frac{\text{ELEV}}{\text{DEPTH}} \text{DESCRIPTION} \left \begin{array}{c} U \\ u \\ v \\ m \end{array} \right \\ \frac{1}{230 \text{ mm}} \text{TOPSOIL} \\ 0.2 \\ \frac{1}{230 \text{ mm}} \text{TOPSOIL} \\ 0.2 \\ \frac{1}{224} \\ \frac{1}{24} \\ \frac{1}{2$		SOIL PROFILE		S	SAMPL	ES	Ľ.	щ	DYNA RESIS	MIC CC	DNE PER	NETRA	TION		DIACT	NAT	URAL				
GROUND SURFACE Image: Constraint of the second se	DEPTH	DESCRIPTION		NUMBER	түре	SPT 'N' VALUE	GROUND WATI CONDITIONS	LEVATION SCAL	SHEA O	R STRE UNCO QUICK	40 (ENGTH NFINED TRIAXI/	<u>50</u> (kPa)	80 1 ♣ FIELI × LAB	D VANE VANE	w _P		TENT w o ONTEN	LIMIT W _L T (%)	γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
0.2 FILL, silty clay, some sand, trace gravel, reddish brown, moist 1 SS			147.			, ",		ш	2	20 4	40 6	50 8	30 1	00	1	0 2	20 :	30	kN/m ³	GR SA S	CL
0.9 SILTY CLAY, some sand, trace	0.2	FILL, silty clay, some sand, trace		1 2A																	
gravel, brown, moist (GLACIAL TILL) containing shale fragments, reddish brown below	0.9	(GLACIAL TILL) containing shale fragments, reddish																			

END OF BOREHOLE

1.5

Unable to drill borehole deeper



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 29

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600200, N: 4828421 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 w 20 100 Wp w ELEV DEPTH ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) (m) γ ○ UNCONFINED● QUICK TRIAXIAL + FIELD VANE \times LAB VANE WATER CONTENT (%) 20 40 60 80 100 20 30 kN/m³ GROUND SURFACE 10 GR SA SI CL 11 150mm TOPSOIL 0.2 FILL, silty clay, some sand, trace gravel, trace rootlets, brown, moist 1 SS 0.6 SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL) 2 SS 1.1 END OF BOREHOLE Unable to drill borehole deeper Borehole was dry and open upon completion of drilling.



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 30

Project No.: 11-13-3148

Date started : June 9, 2014

Sheet No. : 1 of 1

: E: 600177, N: 4828399 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w ELEV DEPTH (m) 20 Wp w ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) γ + FIELD VANE \times LAB VANE ○ UNCONFINED● QUICK TRIAXIAL WATER CONTENT (%) kN/m³ 20 40 60 80 100 10 20 30 GROUND SURFACE GR SA SI CL 11 230mm TOPSOIL 0.2 FILL, silty clay, some sand, trace SS 1 gravel, trace rootlets, brown, moist 0.6 SILTY CLAY, some sand to sandy, trace gravel, brown, moist (GLACIAL TILL) 2 SS SS 0 3 0 22 53 25

END OF BOREHOLE

1.7

Borehole was dry and open upon completion of drilling.

library: library - terraprobe gint.glb report: mto-terraprobe soil (for non-mto jobs) file: 11-13-3148 bh logs gpj



Project : Derry / Argentia Intersection Improvements

Location : Mississauga, Ontario

LOG OF BOREHOLE 31

Project No.: 11-13-3148

Date started : June 6, 2014

Sheet No. : 1 of 1

Positi	on : E: 600127, N: 4828412 (UTM 17	T)			I	Elevatic	on Datu	m : 1	N/A										
Rig ty	pe : CME 75, truck-mounted				I	Drilling	Methoo	1 : 5	Solid s	tem au	ugers								
	SOIL PROFILE	_	S/	AMPL	ES	Ľ.	щ	DYNA RESIS	MIC CO	NE PEN PLOT	NETRA	TION		PLAST	INAT	URAL	LIQUID		
ELEV DEPTH (m)	DESCRIPTION GROUND SURFACE	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	2 SHEA ○	<u>0 4</u> R STRE UNCON QUICK	<u>0</u> 6 NGTH IFINED TRIAXIA	50 (kPa)	80 + FIEI × LAB	100 LD VANE VANE 100		CON TER C	URAL STURE ITENT W -0 ONTEN 20	LIMIT W _L	MEIGHT WEIGHT	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
	120mm ASPHALTIC CONCRETE																		
	600mm FILL-GRAVELLY SAND, some silt, compact, brown, damp		1	SS	21														31 56 <i>(13</i>)
0.7	SILTY CLAY, some sand, trace gravel, very stiff to hard, brown, moist (GLACIAL TILL)		2	SS	22														
1.8			3	SS	45														

END OF BOREHOLE



Project : Derry / Argentia Intersection Improvements

LOG OF BOREHOLE 32

Project No.: 11-13-3148

Date started : June 9, 0204

Loca	tion : Mississauga, Ontario														Sh	eet	No.	1 0	f 1
Positio	on : E: 600127, N: 4828417 (UTM 17	7T)				Elevatio	on Datu	im : N/A	Ą										
Rig typ	be : PIONJAR																		
	SOIL PROFILE		5	SAMPL	ES	Ľ.	щ	DYNAMIC RESISTA	C CON	NE PEN PLOT	NETRA	TION	l	DIACT	NAT	URAL	LIQUIE		
<u>ELEV</u> DEPTH (m)	DESCRIPTION	STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	EVATION SCALE	20 SHEAR S O UN	40 STREM	•) 6	(0 (kPa)	8 <u>0</u> + F	- 100 IELD VANE AB VANE	PLAST LIMIT W _P WA	CON	ITENT W O		λ Weight	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE				0		Ц	20	40) 6	0	80	100	1	0 :	20	30	kN/m ³	GR SA SI CL
0.3	280mm TOPSOIL FILL, silty clay, some sand, trace gravel, trace rootlets, brown, moist		1	SS															
0.6			2	SS															
1.1	END OF BOREHOLE Unable to drill borehole deeper	<u> </u>			1			<u> </u>											



Project : Derry / Argentia Intersection Improvements

LOG OF BOREHOLE 33

Project No.: 11-13-3148

Date started : June 9, 2014

Location : Mississauga, Ontario Sheet No. : 1 of 1 : E: 600102, N: 4828392 (UTM 17T) Position Elevation Datum : N/A PIONJAR Rig type DYNAMIC CONE PENETRATION RESISTANCE PLOT SOIL PROFILE SAMPLES GROUND WATER CONDITIONS PLASTIC NATURAL LIMIT NOISTURE CONTENT ELEVATION SCALE LIQUID LIMIT UNIT WEIGHT REMARKS SPT 'N' VALUE STRAT PLOT & GRAIN SIZE NUMBER 40 60 80 100 w ELEV DEPTH (m) 20 Wp w ΓYPE SHEAR STRENGTH (kPa) DESCRIPTION DISTRIBUTION (%) γ + FIELD VANE \times LAB VANE ○ UNCONFINED● QUICK TRIAXIAL WATER CONTENT (%) kN/m³ 20 40 60 80 100 20 30 GROUND SURFACE 10 GR SA SI CL 11 230mm TOPSOIL 0.2 FILL, silty clay, some sand, trace SS 1 gravel, trace rootlets, brown, moist 0.6 SILTY CLAY, some sand, trace gravel, brown, moist (GLACIAL TILL) 2 SS 1.1 END OF BOREHOLE Unable to drill borehole deeper Borehole was dry and open upon completion of drilling.



Project : Derry / Argentia Intersection Improvements

LOG OF BOREHOLE 34

Project No.: 11-13-3148

Sheet No. :

Date started : June 6, 2014

1 of 1

Location : Mississauga, Ontario

Positio	n : E: 600101, N: 4828401 (UTM 171)				Elevatio	on Datu	im : N/A									
Rig typ	e : CME 75, truck-mounted					Drilling	Method	d : Solid	stem a	ugers	S						
	SOIL PROFILE		S	SAMPL	ES	E	щ	DYNAMIC C RESISTANC	ONE PE E PLOT	NETR	ATION	PLASTIC	NATU MOIST	RAL	LIQUID		
ELEV DEPTH (m)		STRAT PLOT	NUMBER	ТҮРЕ	SPT 'N' VALUE	GROUND WATER CONDITIONS	ELEVATION SCALE	20 SHEAR STR O UNCO ● QUICI	4 <u>0</u> ENGTH NFINED	50 (kPa)	8 <u>0</u> 1 + FIELI × LAB	LIMIT W _P	CONT W O O ER COI		LIMIT W _L	γ κN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)
	GROUND SURFACE 150mm ASPHALTIC CONCRETE													<u> </u>			GR SA SI CL
0.2	650mm FILL-SAND AND GRAVEL, some silt, brown, damp		1	SS	19	_						0					
0.8	FILL, silty clay, some sand, trace gravel, trace organics, stiff, brown, moist		2A 2B	SS	10												
1.2	SILTY CLAY, some sand, trace gravel, very stiff, brown, moist (GLACIAL TILL)		3	SS	22												

END OF BOREHOLE

1.8



Core Photographs

Derry / Argentia Intersection Improvements

11-13-3148

	11-13-3148
	Borehole #8
	Type Core (mm)
11-13-3148	
BH# 8	HL3 50
	HL8 65
	Total 200
	10tai 200
and themes	
PM 1:39 JUL/ 9/2014	
and the second of the second sec	
	Borehole #13
	Type Core (mm)
	HL3 45
11-13-3148	HL8 60
BH# 13	HL8 50
and the second	
H LOAAC PROVIDEN	
	Total 155
PROFESSION CONTRACTOR OF CONTRAC	
Contraction of the second	
PM 1:43 JUL/ 9/2014	
the state of the second s	Borehole #16
	Type Core (mm)
11-13-3148	DFC 65
	HL8 45
BH# 16	
	Tatal 440
	Total 110
	70mm of core lost during coring operation
PM 1:48 JUL/ 9/2014	



Core Photographs

Derry / Argentia Intersection Improvements

11-13-3148

	Borehole #31	11-13-3
	Type Core (mm)	
11 12 21 10	HL3 70	
11-13-3148 PU# 21	HL8 50	
BH# 31		
	Total 120	
AND		

SPL Borehole and Core Logs



	SPL Consultants Lim Geotechnical Environmental Materials Hydro		d		LO	g of	BOR	EHC	DLE I	3H1 1	-1										
PROJ	ECT: Geotechnical Investigation - Derry	/ Roa	d and	d Millc	reek D	rive		DRIL	LING	DATA											
	IT: ROP									id Ster	m Aug	ers									
	ECT LOCATION: Mississauga M: Geodetic									15mm 6/2012	2						EF. NC			78	
	CATION: See Borehole Location Plan							Date.	ouri, i	0/2012	-							0 Z			
	SOIL PROFILE		s	SAMPL	ES			DYNA RESIS	MIC CO TANCE	NE PEN PLOT		TION				URAL	LIQUID		F	REMARKS	
(m)		oT			(0)	GROUND WATER CONDITIONS	_	2	20 4	06	0 ε	30 10	00		C NATU MOIS CON	TURE TENT W		POCKET PEN. (Cu) (kPa)	NATURAL UNIT WT (Mg/m ³)	AND GRAIN SIZE	-
ELEV DEPTH	DESCRIPTION	STRATA PLOT	ER		BLOWS 0.3 m		ELEVATION		AR STI	RENG [®] INED	TH (ki +	Pa) FIELD V. & Sensiti	ANE		(0		OCKET (Cu) (k	IURAL (Mg/n	DISTRIBUTIO (%)	
187.4		STRA	NUMBER	ТҮРЕ	"Z	GROU	ELEV			RIAXIAL	. ×	LAB VA	ANE 50		TER CC 0 2		Г (%) 30	<u>م</u>		GR SA SI (CI
189.9	Topsoil: 75mm	<u>x 1/7</u>	-		-						l										
0.1	FILL: sandy clayey silt, mixed with topsoil, trace rootlets, brown to dark																				~~
	brown, moist, compact		1	SS	12		187								0					3 31 46 2	20
							107														
186.5	CLAYEY SILT: reddish brown,	X																			
0.9	moist, stiff to hard			~~~	10																
			2	SS	10										0						
			-				186														
			3	SS	60									0							
185.3																					
2.1	SHALE: light grey			<u> </u>	50/																
185.1 2.3	END OF BOREHOLE		4	SS	50/ ຈຸບກາກ																-
	Notes: 1) Spoon refusal on bedrock at																				
	2.3m.2) Borehole dry and open upon																				
	completion.																				
		1	I				I		I	I			L	L	L	<u> </u>	I	I			

O ^{8=3%} Strain at Failure

	SPL Consultants Limi Geotechnical Environmental Materials Hydrog		d gy		LO	g of	BOR	EHC	DLE I	3H1 1	-2									
PROJ	ECT: Geotechnical Investigation - Derry I	Road	d and	Millc	reek D	rive		DRIL		DATA										
CLIEN	IT: ROP							Metho	od: Sol	id Ster	n Aug	ers								
	ECT LOCATION: Mississauga								eter: 1								F. NC			78
	M: Geodetic DCATION: See Borehole Location Plan							Date:	Jan/1	6/2012	2					EN	ICL NO	O.: 3		
DITEC	SOIL PROFILE		S	AMPL	ES			DYNA	MIC CO TANCE			TION								DEMARKO
(m)						GROUND WATER CONDITIONS			0 4			0 10	00	PLASTI LIMIT	C MOIS CON	JRAL TURE TENT	LIQUID LIMIT	EN.	NATURAL UNIT WT (Mg/m ³)	REMARKS AND
ELEV	DESCRIPTION	STRATA PLOT	٣		BLOWS 0.3 m	D WA	NO	SHE	AR ST	RENG	TH (ke	2a)		W _P		v >	WL	POCKET PEN. (Cu) (kPa)	RAL UN Mg/m ³)	GRAIN SIZE DISTRIBUTION
DEPTH	DESCRIPTION	RATA	NUMBER	ТҮРЕ			ELEVATION		NCONF		+ ×	FIELD V/ & Sensiti LAB V/	vity NE	WA	TER CC	NTENT	- (%)	00 00	NATUI)	(%)
186.7		S. 1/2	R	≽	"Z	<u>к</u> 0	EL	5	0 10	00 15	50 20	25	50	1	0 2	0 3	0			GR SA SI CL
18 0:0 0.1	FILL: clayey silt to silty clay, trace rootlets, reddish brown, moist, compact		1	SS	13										0					
		\bigotimes					186													
			2	SS	19										∘⊦					
			3	SS	19		185								>			-		
		\bigotimes																		
	decayed wood pieces at 2.4m	\bigotimes	4	SS	14		184								0			-		
		\bigotimes																		
183.0	organics at 3.5 m		5	SS	11											0				
3.7	END OF BOREHOLE																			
	Notes: 1) Borehole dry and open upon completion.																			

SPL SOIL LOG 592-1078.GPJ SPL.GDT 19/3/12

GROUNDWATER ELEVATIONS

 $\frac{\text{GRAPH}}{\text{NOTES}} + {}^3, \times {}^3: \begin{array}{c} \text{Numbers refer} \\ \text{to Sensitivity} \end{array}$

O^{8=3%} Strain at Failure

	SPL Consultants Lin Geotechnical Environmental Materials Hydr	nite ^{rogeolo}	d		LO	g of	BOR	EHC	DLE I	3H1 1	-3									
PROJ CLIEN PROJ	ECT: Geotechnical Investigation - Derr IT: ROP ECT LOCATION: Mississauga M: Geodetic			d Millci	reek Di	rive		Metho Diamo	eter: 1	DATA id Ster 15mm 3/2012	-	ers					EF. NO			78
BHLC	OCATION: See Borehole Location Plan																			
	SOIL PROFILE		s	AMPL	ES			DYNA	MIC CO	NE PEN PLOT	IETRA	TION			NATI	IDAL				REMARKS
(m) ELEV DEPTH	DESCRIPTION	STRATA PLOT	NUMBER	түре	"N" <u>BLOWS</u> 0.3 m	GROUND WATER CONDITIONS	ELEVATION	2 SHEA O UI ● QI	0 4 AR STI NCONF JICK TF	0 6 RENG	0 8 TH (kF + ×	0 10	ANE vity ANE	W _P I WAT			LIQUID LIMIT W _L	POCKET PEN. (Cu) (kPa)	NATURAL UNIT WI (Mg/m ³)	AND GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
185.2 0.0	FILL: sand and gravel over 50mm	X	~	-	-	00	ш													GR SA SI OL
	thick brick, brown, moist, compact						185								ļ					
184.9 0.3	CLAYEY SILT: reddish brown,	- HXX	1	SS	13										0					
0.0	moist, stiff to hard																			
			\vdash		50/															
			2	SS	100mm									0						
102.0							184													
183.9 18 3 :9	SHALE: light grey	111	-	. SS .	50/															
1.4	END OF BOREHOLE		\sim		50mm										l					
	Notes: 1) Spoon refusal on bedrock at																			
	1.4m. 2) Borehole dry and open upon																			
	completion.																			

Derry Rd & Millcreek Dr. Mississauga



CORE NO.: 1

LOCATION:

DESCRIPTION: Good bond between lift 1 and lift 2

LIFT THICKNESSES: Lift 1: 30 mm Lift 2: 89 mm

AVERAGE THICKNESS: 119 mm

CORE NO.: 2

LOCATION:

DESCRIPTION: Good bond between lift 1 and lift 2

LIFT THICKNESSES: Lift 1: 30 mm Lift 2: 89 mm

AVERAGE THICKNESS: 119 mm



Derry Rd & Millcreek Dr. Mississauga



CORE NO.: 3

LOCATION:

DESCRIPTION: Good bond between lift 1 and lift 2

LIFT THICKNESSES: Lift 1: 25 mm Lift 2: 100 mm

AVERAGE THICKNESS: 125 mm

CORE NO.: 4

LOCATION:

DESCRIPTION: Good bond between lift 1 and lift 2

LIFT THICKNESSES: Lift 1: 20 mm Lift 2: 99 mm

AVERAGE THICKNESS: 119 mm



Derry Rd & Millcreek Dr. Mississauga



CORE NO.: 9

LOCATION:

DESCRIPTION: Good bond between lift 1 and lift 2

LIFT THICKNESSES: Lift 1: 30 mm Lift 2: 76 mm

AVERAGE THICKNESS: 106 mm



CORE NO.: 10

LOCATION:

DESCRIPTION: 1 lift

LIFT THICKNESSES: Lift 1: 75 mm

AVERAGE THICKNESS: 75 mm

Derry Rd & Millcreek Dr. Mississauga



CORE NO.: 11

LOCATION:

DESCRIPTION: 1 lift (Concrete)

LIFT THICKNESSES: Lift 1: 138 mm

AVERAGE THICKNESS: 138 mm

CORE NO.: 12

LOCATION:

DESCRIPTION: 1 lift (Concrete)

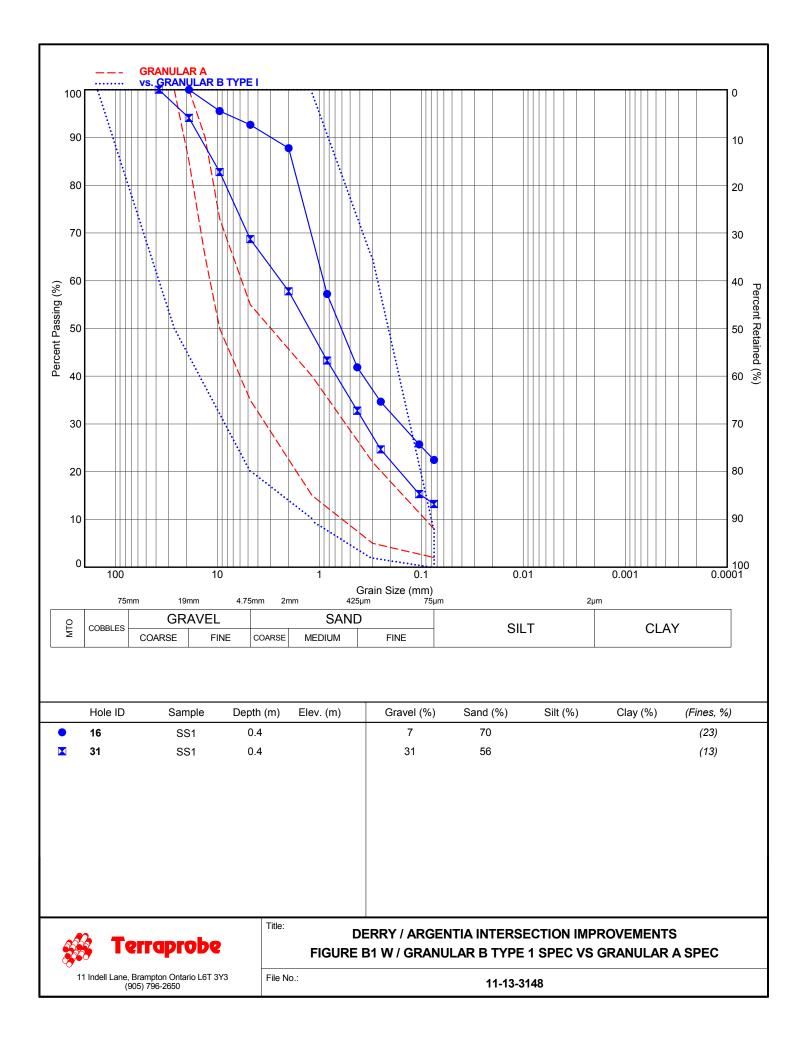
LIFT THICKNESSES: Lift 1: 150 mm

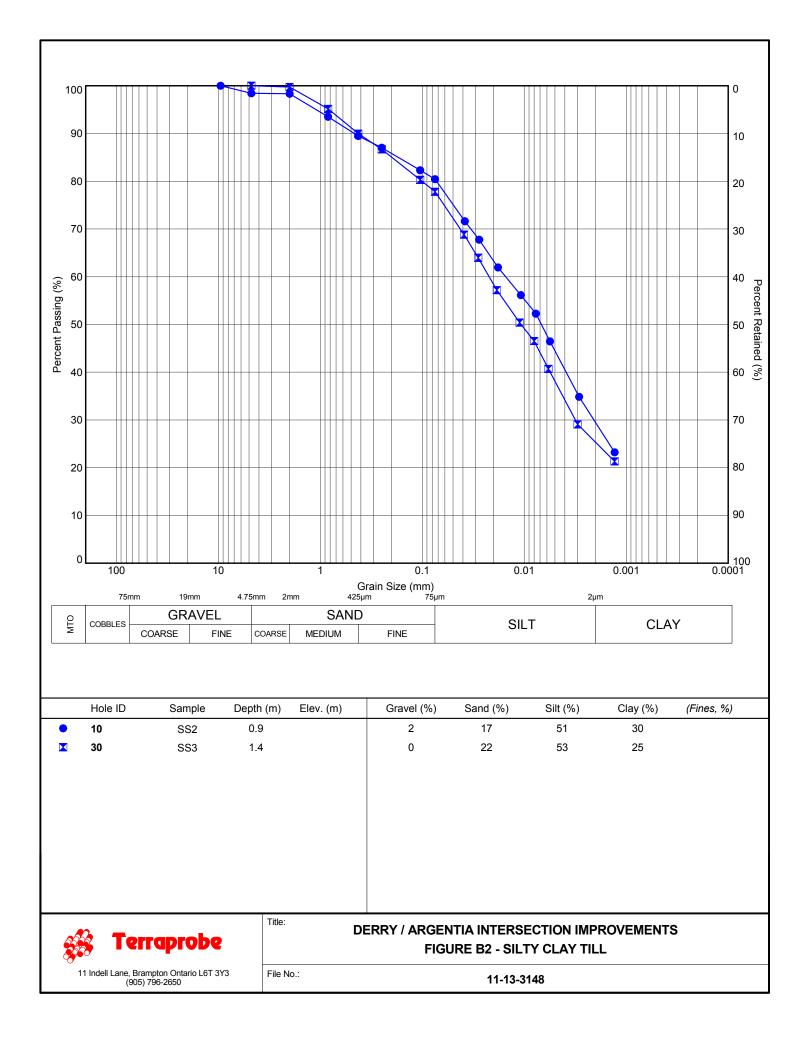
AVERAGE THICKNESS: 150 mm



APPENDIX B Laboratory Test Results







APPENDIX C Flexible Pavement Condition Evaluation Forms



Flexible Pavement Condition Evaluation Form

Ministry of Transportation

😵 Ontario

Loc	ation:		Der	ry Ro	bad \	Nest	, Mis	ssiss	saug	a, Oi	ntario	0					_	District		Hi	ghway					
Fro	m:	East Limit (Sta. 9+720)				To:				Wes	t Lir	nit (S	Sta.	10+1	166)										
LH	RS	haring		•		km		Se	ectio	on L	eng	th		4	4	6 m	-	Traffic Direction	В		directior bound; V			d; S - so	uthboun	d;
Su	rvey Date	begins 1 4 year	offs 08 month	PC	R		7	0]	RC	R [7	•	0]			Facility	А	O - othe	anes; C - ers (additi	onal lan	es)			
Co	ntract No.	-		W	/P N	lo.												Class	А	F - freev S - seco	way; A - a ondary	arterial; (C - collec	tor; L - I	ocal;	
		□ 10	Excellent (smoo	th)		everi	ty of ∣	Distre			ensity ent of			e %		S	Shou	Ilders			rity of ress			-	Distres	
	de	- 8	Good (comfortat		Slight	÷	ate	a	Very Severe	>	Intermittent	ent	sive	Throughout			Ι		Ri	ght	Le	eft	Rig	aht	Le	eft
	ondition ating	- 6	Fair (uncomfortal		ry SI	Slight	Moderate	Severe	/ Se	Few	ermi	Frequent	Extensive	roug		Dominant		Distress	Mod.	Sev.	Mod.	Sev.	10-30	>30	10-30	>30
	t 80 km/hr)	- 4	Poor (v. rough/bu	mpy)	Very		ĕ	S	Ver		Int	ш	ш	μ		Туре			1	2	1	2	1	2	1	2
			Very Poor, (dange	rous,						0	20	50	80	00	11	Paved		Cracking								
		<u> </u>	at 80 km/hr)							<10	10-20	20-50	50-80	80-100		Full	v	Pavement Edge/								
		PAVEMENT			1	2	3	4	5	1	2	3	4	5		Paved		Curb Separation								
	Surface	Ravelling &	C. Agg. Loss	1		~					~					Partial		Distortion								
	Defects	Flushing		2												Surface		Breakup/Separtion								
	Surface	Rippling an	d Shoving	3			<u> </u>									Treated		Edge Break								
	Deformations	Wheel Trac	k Rutting	4	<u> </u>	√	.				~					Primed		Breakup/Separtion								
		Distortion		5												Gravel										
	Longitudinal	Single and	Multiple	6	_	~					~				.											
	Wheel Track	Alligator		7													Mair	ntenance			EXT	ENT OF C	OCCURRE	NCE, %		
	Centre Line	Single and	Multiple	8	_	.	.											atment		<10	10-20) .	20-50	50-80)	>80
Q		Alligator		9																1	2		3	4		5
CRACKING	Pavement	Single and	Multiple	10	.	 	 											Manual Patching								
RAC	Edge	Alligator		11														Machine Patching								
с О	Transverse	Half, Full ar	nd Multiple	12		✓					\checkmark					Pavement		Spray Patching			~					
	Indiroveree	Alligator		13													F	Rout and Seal Crack	s		✓					
	Longitudinal Me	ander and Midl	ane	14														Chip Seal								
	Random / Map			15														Manual Patching								
																Shoulders		Machine Patching								
Dief	ress Comment	e: (itoma not	covered above)													GIUUIUEIS	F	Rout and Seal Crack	s							
5151		.a. (IICIIIS IIOL																Chip Seal								
Der	ry Road west leg	g recently repa	aved and is in e	xcelle	ent c	ondi	tion.								-	Other Comm	ents:	e (e.g., subsections,	additional	contracts)					

Evaluated by: Hussein Ahmed, P. Eng.

Flexible Pavement Condition Evaluation Form

Ministry of Transportation

😵 Ontario

Loc	ation:	Arç	genti	a Ro	oad,	Miss	issa	uga,	Ont	ario						-	District		Ні	ghway					
From	m:	South Limit (Sta. 1+790)				To:				Nor	th Li	mit ((Sta	. 2+2	280)				J						
LH	RS		•		km		Se	ectio	on L	.eng	lth		4	9	0 m	-	Traffic Direction	В		directior bound; V	,		d; S - so	uthboun	d;
Su	rvey Date	begins offs 1 4 0 8 year month	PC	R		7	0]	RC	R	7	•	0]			Facility	А	O - othe	anes; C - ers (addit	ional lan	es)			
Со	ntract No.		W	/P N	lo.												Class	С	F - freev S - seco	way; A - a ondary	arterial; (C - collec	tor; L - l	ocal;	
		Excellent (smoot	h)		everi	ty of [Distre	I		ensity ent of		rrence	e %		Ş	Shou	Ilders			rity of ress			ensity of nt of Oc		
	de	Good (comfortab		Slight	Ŧ	ate	e	Very Severe	v	Intermittent	ent	Extensive	Throughout			T		Ri	ight	Le	eft	Rig	aht	Le	eft
	ondition ating	Fair (uncomfortab	,	Very S	Slight	Moderate	Severe	y Se	Few	ermi	Frequent	xten:	roug		Dominant		Distress	Mod.	Sev.	Mod.	Sev.	10-30	>30	10-30	>30
	t 80 km/hr)	Poor (v. rough/bun	npy)	<e <<="" td=""><td></td><td>Ň</td><td>0</td><td>Ver</td><td></td><td>Int</td><td>ш</td><td>Ш</td><td>Ц</td><td></td><td>Туре</td><td></td><td></td><td>1</td><td>2</td><td>1</td><td>2</td><td>1</td><td>2</td><td>1</td><td>2</td></e>		Ň	0	Ver		Int	ш	Ш	Ц		Туре			1	2	1	2	1	2	1	2
		Very Poor, (danger	ous,						0	10-20	50	50-80	00		Paved		Cracking								
		└── ⁰ at 80 km/hr)							<10	10-	20-50	50-	80-100		Full	N	Pavement Edge/								
		PAVEMENT		1	2	3	4	5	1	2	3	4	5		Paved		Curb Separation								
	Surface	Ravelling & C. Agg. Loss	1			~					~				Partial		Distortion								
	Defects	Flushing	2												Surface		Breakup/Separtion								
	Surface	Rippling and Shoving	3	_	.										Treated		Edge Break								
	Deformations	Wheel Track Rutting	4	 	~					~					Primed		Breakup/Separtion								
		Distortion	5												Gravel	<u> </u>									
	Longitudinal	Single and Multiple	6	_	~					~															
	Wheel Track	Alligator	7													Mair	ntenance					OCCURRE			
	Centre Line	Single and Multiple	8	 	.												atment		<10	10-20)	20-50	50-80)	>80
ġ		Alligator	9													1			1	2		3	4		5
CRACKING	Pavement	Single and Multiple	10	 	 												Manual Patching								
RAC	Edge	Alligator	11			✓				~							Machine Patching								
0	Transverse	Half, Full and Multiple	12	 	✓					~					Pavement		Spray Patching								
		Alligator	13													F	Rout and Seal Cracl	ks		~					
	Longitudinal Me	ander and Midlane	14	_	<u> </u>												Chip Seal								
	Random / Map		15														Manual Patching								
															Shoulders		Machine Patching								
Dist	ress Comment	s: (items not covered above)														F	Rout and Seal Cracl	ks							
5.30														_			Chip Seal								
														_	Other Comm	ents:	: (e.g., subsections,	additiona	l contracts	;)					

Evaluated by: Hussein Ahmed, P. Eng.

APPENDIX D Certificate of Chemical Analysis (Soil Chemistry)





CLIENT NAME: TERRAPROBE INC. 11 INDELL LANE BRAMPTON, ON L6T3Y3 (905) 796-2650

ATTENTION TO: Hussein Ahmed

PROJECT: 11-13-3148

AGAT WORK ORDER: 14T852410

SOIL ANALYSIS REVIEWED BY: Sofka Pehlyova, Senior Analyst

DATE REPORTED: Jun 20, 2014

PAGES (INCLUDING COVER): 5

VERSION*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

*NOTES	

All samples will be disposed of within 30 days following analysis. Please contact the lab if you require additional sample storage time.

AGAT Laboratories (V1)

Member of: Association of Professional Engineers, Geologists and Geophysicists of Alberta (APEGGA) Western Enviro-Agricultural Laboratory Association (WEALA) Environmental Services Association of Alberta (ESAA) AGAT Laboratories is accredited to ISO/IEC 17025 by the Canadian Association for Laboratory Accreditation Inc. (CALA) and/or Standards Council of Canada (SCC) for specific tests listed on the scope of accreditation. AGAT Laboratories (Mississauga) is also accredited by the Canadian Association for Laboratory Accreditation Inc. (CALA) for specific drinking water tests. Accreditations are location and parameter specific. A complete listing of parameters for each location is available from www.cala.ca and/or www.scc.ca. The tests in this report may not necessarily be included in the scope of accreditation.

Page 1 of 5



Certificate of Analysis

AGAT WORK ORDER: 14T852410 PROJECT: 11-13-3148 5835 COOPERS AVENUE MISSISSAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 http://www.agatlabs.com

CLIENT NAME: TERRAPROBE INC.

ATTENTION TO: Hussein Ahmed

O. Reg. 153(511) - Metals & Inorganics (Soil)

DATE RECEIVED: 2014-06-16

DATE RECEIVED: 2014-06-16						DATE REPORTED: 2014-06-20
		SAMPLE DESCRI	PTION: BF	H17/SS2B	BH25/SS1	
		SAMPLE	TYPE:	Soil	Soil	
		DATE SAM	IPLED: 6/	/13/2014	6/13/2014	
Parameter	Unit	G/S	RDL 5	5481141	5481159	
Antimony	µg/g	1	0.8	<0.8	<0.8	
Arsenic	µg/g	11	1	6	6	
Barium	µg/g	210	2	80	78	
Beryllium	µg/g	2.5	0.5	0.6	0.7	
Boron	µg/g	36	5	14	9	
Boron (Hot Water Soluble)	µg/g	NA	0.10	0.28	0.19	
Cadmium	µg/g	1	0.5	<0.5	<0.5	
Chromium	µg/g	67	2	21	19	
Cobalt	µg/g	19	0.5	12.0	10.6	
Copper	µg/g	62	1	20	23	
ead	µg/g	45	1	10	10	
Nolybdenum	µg/g	2	0.5	0.8	<0.5	
lickel	µg/g	37	1	26	23	
Selenium	µg/g	1.2	0.4	<0.4	<0.4	
Silver	µg/g	0.5	0.2	<0.2	<0.2	
Thallium	µg/g	1	0.4	<0.4	<0.4	
Jranium	µg/g	1.9	0.5	0.5	<0.5	
/anadium	µg/g	86	1	27	26	
Zinc	µg/g	290	5	60	58	
Chromium VI	µg/g	0.66	0.2	<0.2	<0.2	
Cyanide	µg/g	0.051 (0.040	<0.040	<0.040	
Mercury	µg/g	0.16	0.10	<0.10	<0.10	
Electrical Conductivity (2:1)	mS/cm	0.47 0	0.005	2.35	0.146	
Sodium Adsorption Ratio (2:1)	NA	1	NA	50.3	0.630	
pH, 2:1 CaCl2 Extraction	pH Units			8.12	7.74	

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard: Refers to T1(AG) - Current

5481141-5481159 EC & SAR were determined on the DI water extract obtained from the 2:1 leaching procedure (2 parts DI water:1 part soil). pH was determined on the 0.01M CaCl2 extract prepared at 2:1 ratio.

Certified By:

Sofiea Pehlyora

DATE REPORTED: 2014-06-20

	<mark>AGAT</mark>	Laboratories	Guideline Violation AGAT WORK ORDER: 14T8524 PROJECT: 11-13-3148	-	MISSIS - F	OOPERS AVENUE SAUGA, ONTARIO CANADA L4Z 1Y2 TEL (905)712-5100 FAX (905)712-5122 www.aqatlabs.com
CLIENT NAME	: TERRAPROBE INC.			ATTENTION TO: Hussein Ahmed		www.agaliabs.com
SAMPLEID	SAMPLE TITLE	GUIDELINE	ANALYSIS PACKAGE	PARAMETER	GUIDEVALUE	RESULT
5481141	BH17/SS2B	T1(AG) - Current	O. Reg. 153(511) - Metals & Inorganics (Soil)	Electrical Conductivity (2:1)	0.47	2.35

Sodium Adsorption Ratio (2:1)

O. Reg. 153(511) - Metals & Inorganics (Soil)

T1(AG) - Current

5481141

BH17/SS2B

50.3



Quality Assurance

CLIENT NAME: TERRAPROBE INC.

PROJECT: 11-13-3148

AGAT WORK ORDER: 14T852410 ATTENTION TO: Hussein Ahmed

				Soi	l Ana	alysis	;								
RPT Date: Jun 20, 2014			C	UPLICATE	Ξ		REFEREN	NCE MA	TERIAL	METHOD	BLANK	SPIKE	MAT	RIX SPI	KE
PARAMETER	Batch	Sample Id	Dup #1	Dup #2	RPD	Method Blank	Measured		eptable nits	Recovery		ptable nits	Recovery		eptable nits
		lu					Value	Lower	Upper		Lower	Upper		Lower	Upper
O. Reg. 153(511) - Metals & Inor	ganics (Soil)	1													
Antimony	1		< 0.8	< 0.8	0.0%	< 0.8	106%	70%	130%	98%	80%	120%	98%	70%	130%
Arsenic	1		4	4	0.0%	< 1	114%	70%	130%	101%	80%	120%	102%	70%	130%
Barium	1		117	118	0.9%	< 2	97%	70%	130%	87%	80%	120%	89%	70%	130%
Beryllium	1		0.7	0.8	13.3%	< 0.5	102%	70%	130%	104%	80%	120%	94%	70%	130%
Boron	1		7	7	0.0%	< 5	80%	70%	130%	106%	80%	120%	96%	70%	130%
Boron (Hot Water Soluble)	5481141 5	5481141	0.28	0.28	0.0%	< 0.10	112%	60%	140%	103%	70%	130%	95%	60%	140%
Cadmium	1		< 0.5	< 0.5	0.0%	< 0.5	89%	70%	130%	104%	80%	120%	101%	70%	130%
Chromium	1		22	22	0.0%	< 2	94%	70%	130%	98%	80%	120%	101%	70%	130%
Cobalt	1		10.6	10.6	0.0%	< 0.5	95%	70%	130%	98%	80%	120%	93%	70%	130%
Copper	1		18	17	5.7%	< 1	103%	70%	130%	104%	80%	120%	93%	70%	130%
Lead	1		15	14	6.9%	< 1	97%	70%	130%	96%	80%	120%	91%	70%	130%
Molybdenum	1		0.5	0.5	0.0%	< 0.5	114%	70%	130%	104%	80%	120%	108%	70%	130%
Nickel	1		20	20	0.0%	< 1	106%	70%	130%	104%	80%	120%	97%	70%	130%
Selenium	1		0.4	0.5	22.2%	< 0.4	99%	70%	130%	101%	80%	120%	101%	70%	130%
Silver	1		< 0.2	< 0.2	0.0%	< 0.2	107%	70%	130%	114%	80%	120%	111%	70%	130%
Thallium	1		< 0.4	< 0.4	0.0%	< 0.4	105%	70%	130%	108%	80%	120%	99%	70%	130%
Uranium	1		0.6	0.6	0.0%	< 0.5	92%	70%	130%	98%	80%	120%	98%	70%	130%
Vanadium	1		31	31	0.0%	< 1	92%	70%	130%	96%	80%	120%	95%	70%	130%
Zinc	1		71	70	1.4%	< 5	98%	70%	130%	101%	80%	120%	91%	70%	130%
Chromium VI	1		< 0.2	< 0.2	0.0%	< 0.2	97%	70%	130%	94%	80%	120%	100%	70%	130%
Cyanide	1		< 0.040	< 0.040	0.0%	< 0.040	100%	70%	130%	99%	80%	120%	109%	70%	130%
Mercury	1		< 0.10	< 0.10	0.0%	< 0.10	114%	70%	130%	97%	80%	120%	95%	70%	130%
Electrical Conductivity (2:1)	1		0.137	0.139	1.4%	< 0.005	101%	90%	110%	NA			NA		
Sodium Adsorption Ratio (2:1)	1		15.5	15.4	0.6%	NA	NA			NA			NA		
pH, 2:1 CaCl2 Extraction	1		7.30	7.34	0.5%	NA	100%	80%	120%	NA			NA		

Comments: NA signifies Not Applicable.

Certified By:

Sofrea Pehlyora

Page 4 of 5

AGAT QUALITY ASSURANCE REPORT (V1)

AGAT Laboratories is accredited to ISO/IEC 17025 by the Canadian Association for Laboratory Accreditation Inc. (CALA) and/or Standards Council of Canada (SCC) for specific tests listed on the scope of accreditation. AGAT Laboratories (Mississauga) is also accredited by the Canadian Association for Laboratory Accreditation Inc. (CALA) for specific tests tests. Accreditations are location and parameter specific. A complete listing of parameters for each location is available from www.cala.ca and/or www.scc.ca. The tests in this report may not necessarily be included in the scope of accreditation.



Method Summary

CLIENT NAME: TERRAPROBE INC.

PROJECT: 11-13-3148

AGAT WORK ORDER: 14T852410 ATTENTION TO: Hussein Ahmed

PROJECT: 11-13-3148		ATTENTION TO:	Hussein Ahmed
PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE
Soil Analysis		L	-
Antimony	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Arsenic	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Barium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Beryllium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Boron	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Boron (Hot Water Soluble)	MET-93-6104	EPA SW 846 6010C; MSA, Part 3, Ch.21	ICP/OES
Cadmium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Chromium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Cobalt	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Copper	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Lead	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Molybdenum	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Nickel	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Selenium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Silver	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Thallium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Uranium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Vanadium	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Zinc	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Chromium VI	INOR-93-6029	SM 3500 B; MSA Part 3, Ch. 25	SPECTROPHOTOMETER
Cyanide	INOR-93-6052	MOE CN-3015 & E 3009 A;SM 4500 CN	TECHNICON AUTO ANALYZER
Mercury	MET-93-6103	EPA SW-846 3050B & 6020A	ICP-MS
Electrical Conductivity (2:1)	INOR-93-6036	McKeague 4.12, SM 2510 B	EC METER
Sodium Adsorption Ratio (2:1)	INOR-93-6007	McKeague 4.12 & 3.26 & EPA SW-846 6010B	ICP/OES
pH, 2:1 CaCl2 Extraction	INOR-93-6031	MSA part 3 & SM 4500-H+ B	PH METER